

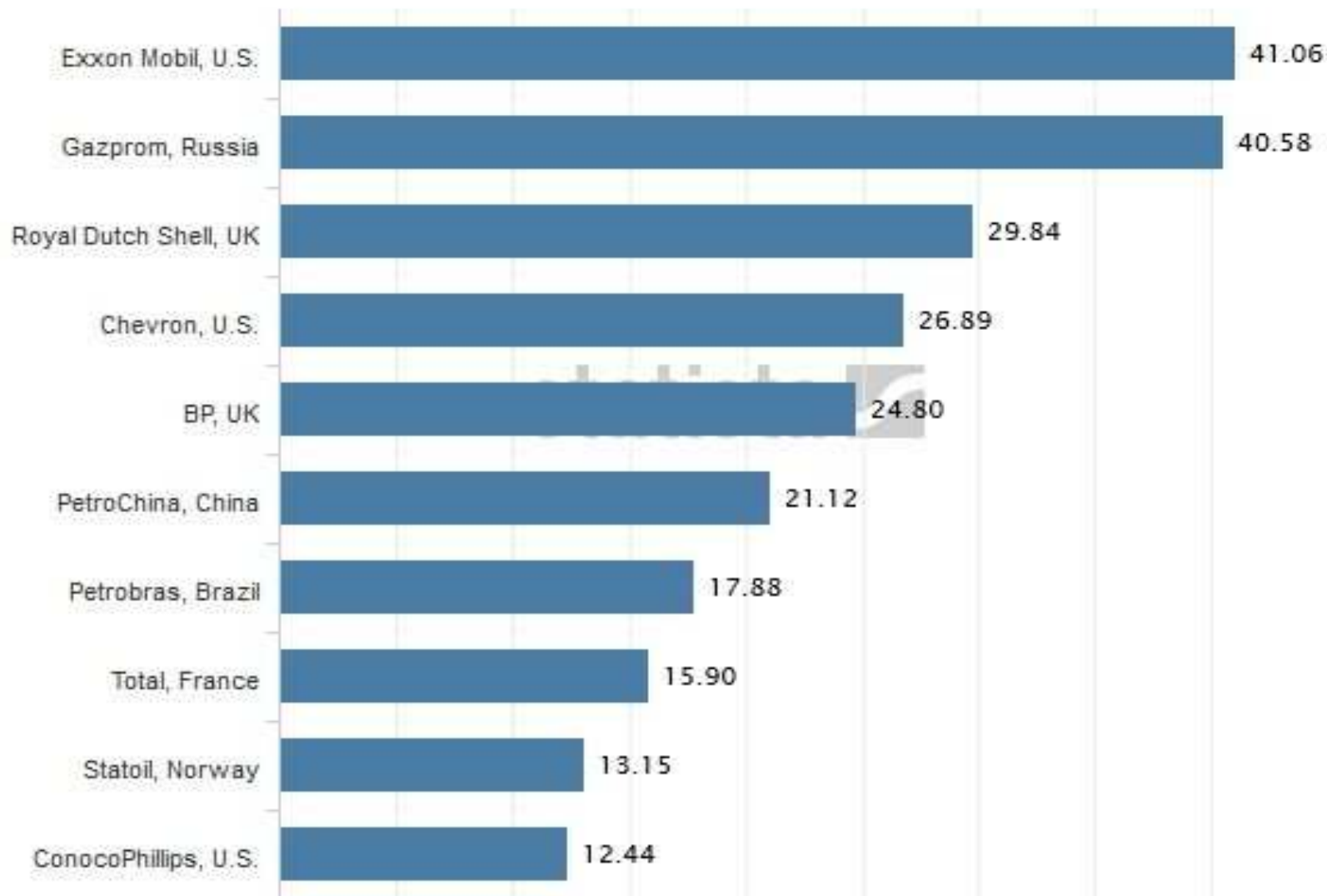
Oil corporations

The seven sisters were the following:

1. Standard Oil of New Jersey (Esso), which merged with Mobil to form ExxonMobil.
2. Royal Dutch Shell Anglo-Dutch
3. British Anglo-Persian Oil Company (APOC). This later became BP then BP Amoco following a merger with Amoco (which in turn was formerly Standard Oil of Indiana). It is now known solely by the initials BP.
4. Standard Oil of New York (Socony). This later became Mobil, which merged with Exxon to form ExxonMobil.
5. Standard Oil of California (Socal). This became Chevron, then, upon merging with Texaco, ChevronTexaco. It has since dropped the 'Texaco' suffix, returning to Chevron.
6. Gulf Oil. Most of this became part of Chevron, with smaller parts becoming part of BP, and Cumberland Farms.
7. Texaco. Merged with Chevron in 2001.

Rank	Company	Global 500 rank	REVENUES		PROFITS	
			\$ millions	% change from 2008	\$ millions	% change from 2008
1	Exxon Mobil	2	372,824	7	40,610	3
2	Royal Dutch Shell	3	355,782	12	31,331	23
3	BP	4	291,438	6	20,845	-5
4	Chevron	6	210,783	5	18,688	9
5	Total	8	187,280	11	18,042	22
6	ConocoPhillips	10	178,558	4	11,891	-24
7	Sinopec	16	159,260	21	4,166	13
8	China National Petroleum	25	129,798	17	14,925	13
9	ENI	27	120,565	11	13,703	19
10	Valero Energy	49	96,758	6	5,234	-4
11	Statoil Hydro	59	89,224	35	7,526	19
12	Petrobras	63	87,735	21	13,138	2
13	SK Holdings	86	70,717	20	1,505	3
14	Lukoil	90	67,205	23	9,511	27
15	Repsol YPF	92	67,006	10	4,364	11
16	Petronas	95	66,218	30	18,118	41

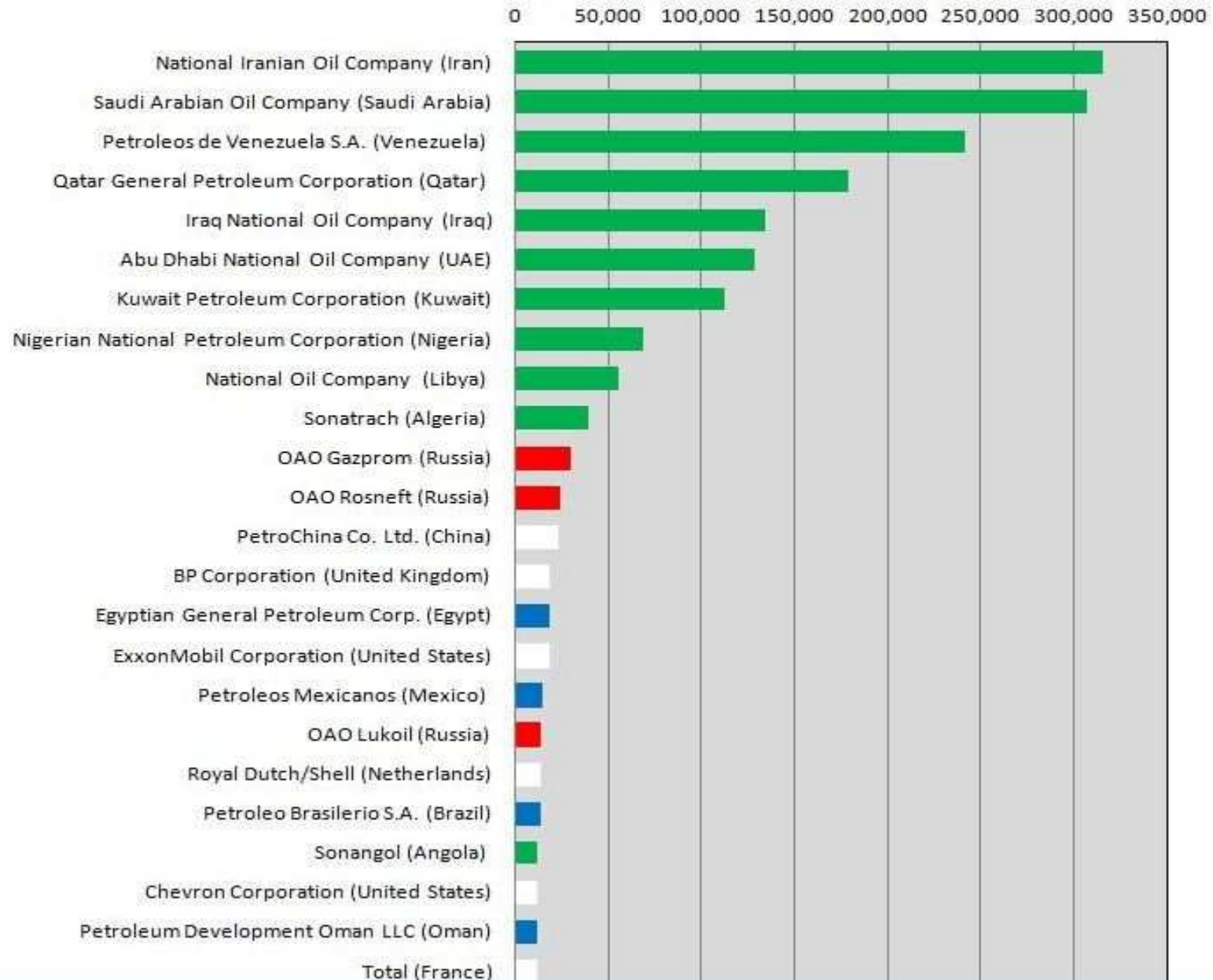
2012 ranking of the global top 10 oil and gas companies based on net income (in billion U.S. dollars)



Net income in billion U.S. dollars

World's Largest Oil and Gas Companies

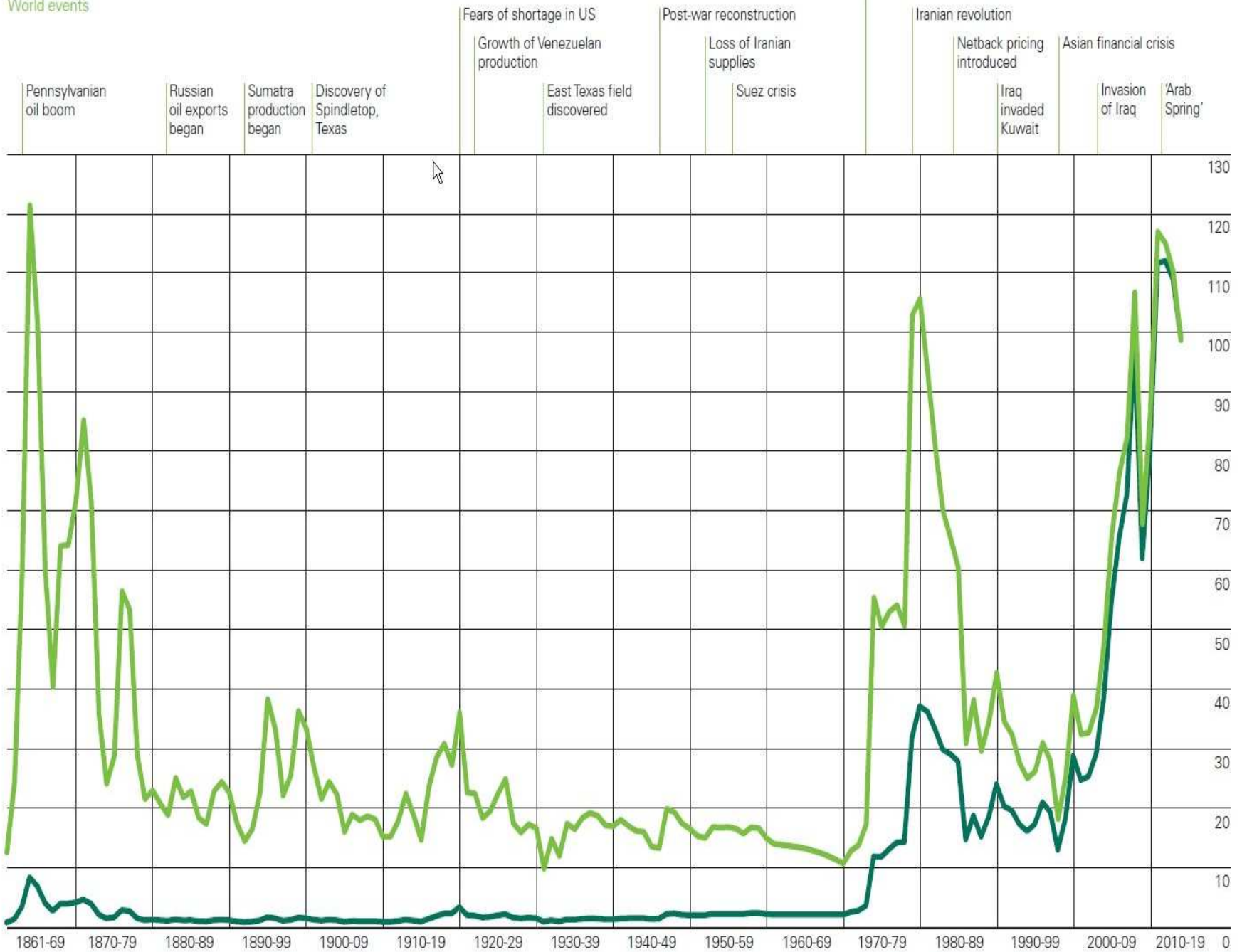
Million Oil Equivalent Barrels



Crude oil prices 1861-2014

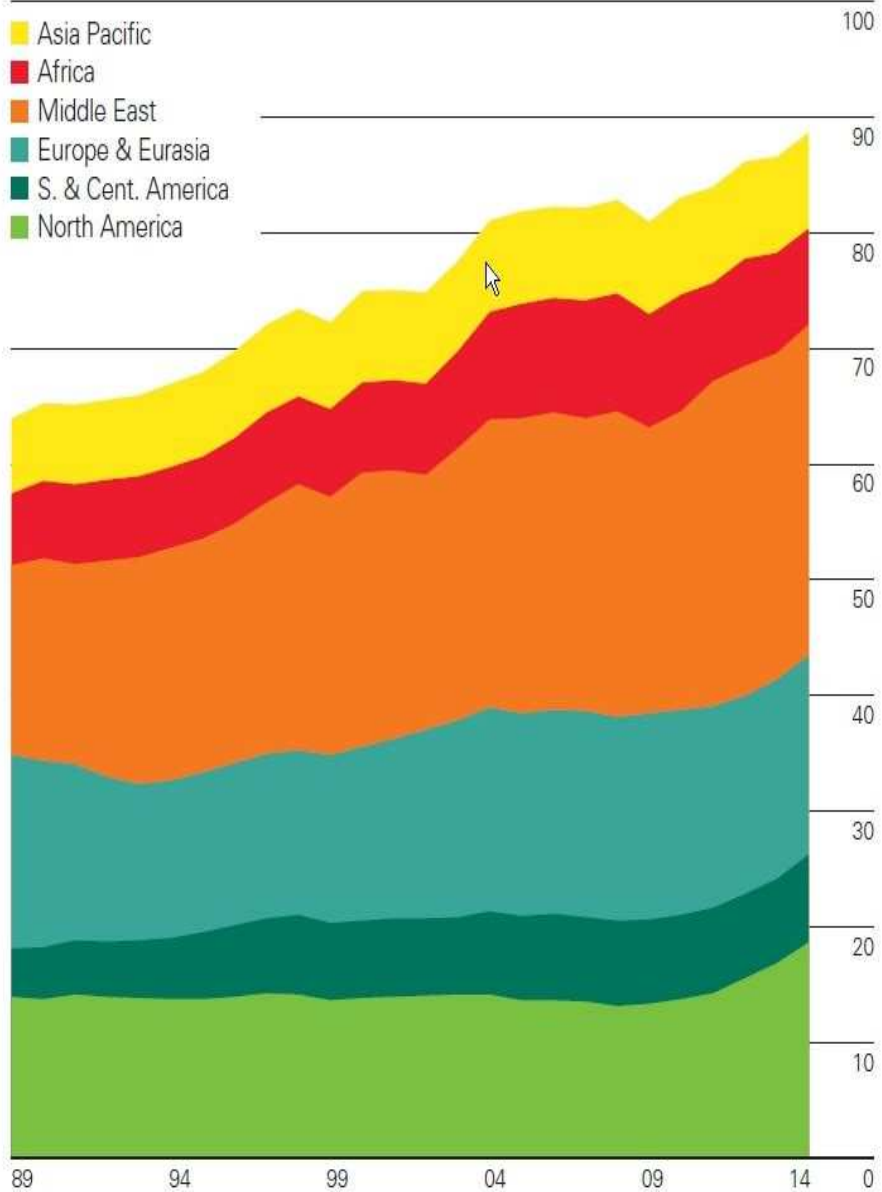
US dollars per barrel

World events



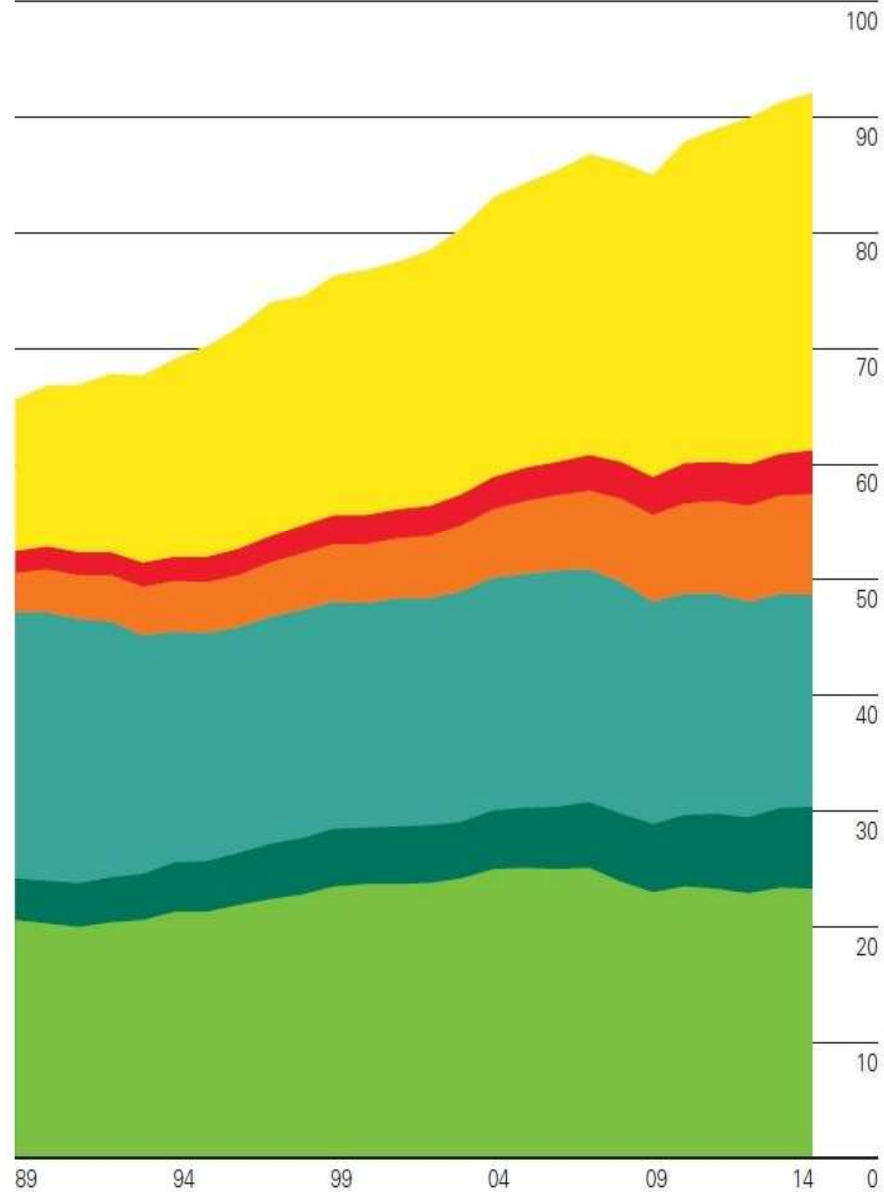
Production by region

Million barrels daily



Consumption by region

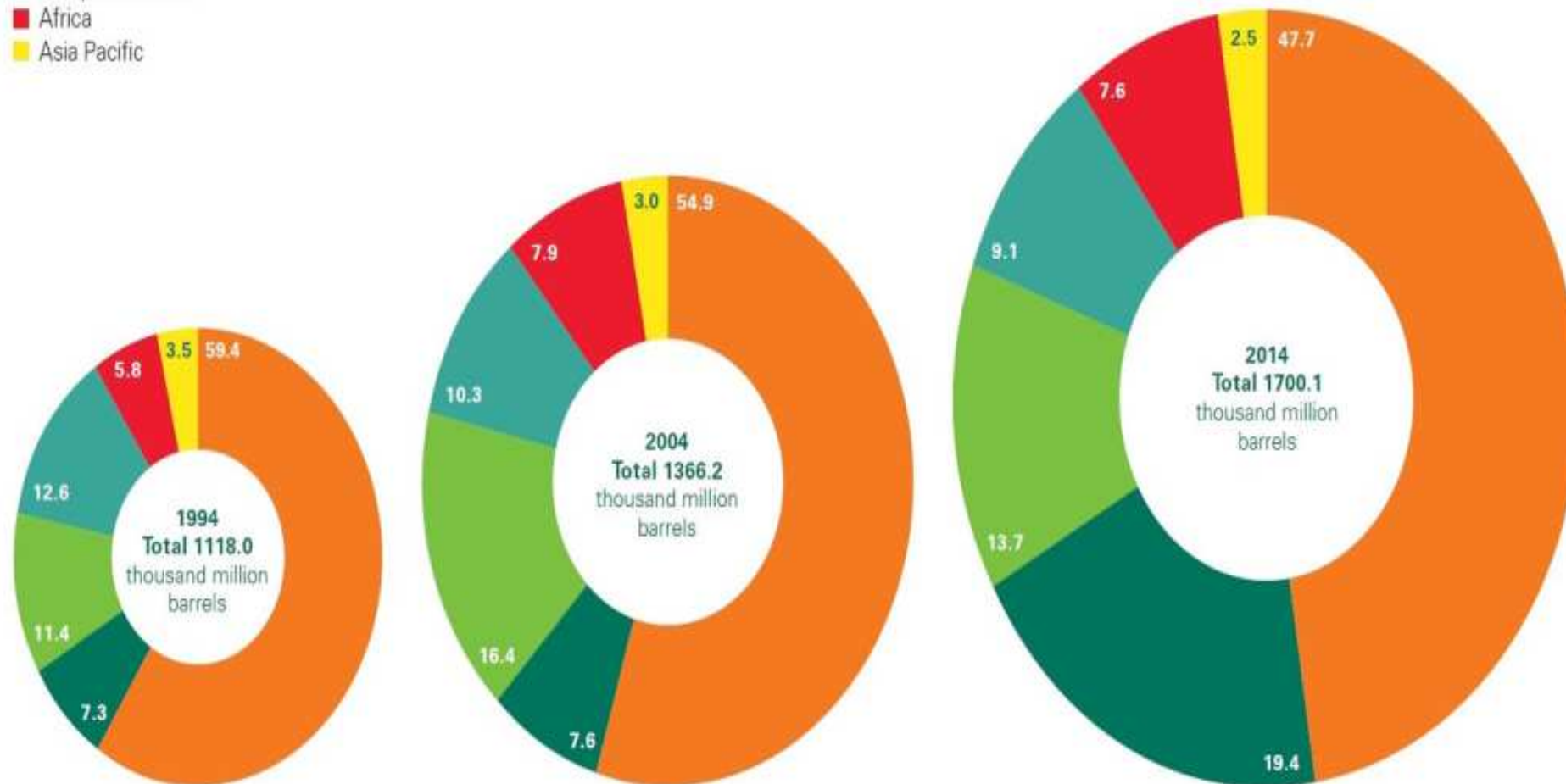
Million barrels daily



Distribution of proved reserves in 1994, 2004 and 2014

Percentage

- Middle East
- S. & Cent. America
- North America
- Europe & Eurasia
- Africa
- Asia Pacific



Crude Oil and its Products

הנפט הוא תערובת של פחממנים פרפינים, ארומטיים ונפתנים,
עם מעט תרכבות חנקן וגפרית.
הרכב הנפט שונה לפי מקורו.
מוערך שהמקור הקדום היה בעלי חיים +
צמחיה מלפני הרבה מליוני שנים.

בזיקוק ישיר של הנפט מפרידים את הפרקציות הבאות:
גפ"ס
גזולין, נפתה וממיסים
קרוסין ודלק מטוסים
סולר ודלק דיזל
מזוט
שמני סיכה ואספלט.

תהליכי השבחת נפט כוללים:
פיצוח תרמי ופיצוח מימני
פרוס תרמי
אלקילציה
איזומריזציה
פולימריזציה

‣ מבין מוצרי הזיקוק הראשוני של נפט החשוב ביותר הוא הנפתה המשמש חומר גלם לגזולין וכן חומר הזנה לתהליכי יצור אתילן, פרופילן וחמרים ארומטיים. את הפרקציה הארומטית מפרידים מנפתה בתהליכי מיצוי.

‣ ממוצרי נפט מפרידים מספר תרכובות נקיות המהוות חמרי גלם לרב מוצרי התעשייה הפטרוכימית:

‣ אתילן

‣ פרופילן

‣ בנזן

‣ טולואן

‣ אורתו קסילן ופרה קסילן

‣ נפתלן

‣ כתחליפים לנפט גלמי מציעים חמרי טבע, בעיקר סוכר, ממנו הצליחו להפיק מוצרים רבים אבל לא במחיר סביר. אצטילן, הניתן להפקה מפחם, שימש כחומר הגלם העיקרי לתעשייה הפטרוכימית בגרמניה במלחמת העולם השנייה.

‣ גז סינתזה, תערובת של CO ומימן, הוא חומר גלם חשוב לתהליכים רבים. כיום מיצרים אותו בעיקר בחמצון חלקי של מתן או של נפתה בעיקר ליצור מתנול ואמוניה, ניתן ליצר גז סינתזה בחמצון חלקי של פחם. מגז סינתזה מפחם ניתן ליצר חומר דמוי נפט טבעי ומספר רב של תהליכים פותחו למטרה זו ואחדים מתהליכים אלה זכו למספר רב של ישומים, אך מחירי הנפט שצוללו עצרו ישומים נוספים.

$(141.5/S.G.) - 131.5 = \text{API Gravity}$

Typical analysis of some crude oils

	Arab Extra Light*	Alameen Egypt	Arab Heavy	Bakr-9 Egypt
Gravity, °API	38.5	33.4	28.0	20.9
Carbon residue (wt %)	2.0	5.1	6.8	11.7
Sulfur content (wt %)	1.1	0.86	2.8	3.8
Nitrogen content (wt %)	0.04	0.12	0.15	—
Ash content (wt %)	0.002	0.004	0.012	0.04
Iron (ppm)	0.4	0.0	1.0	—
Nickel (ppm)	0.6	0.0	9.0	108
Vanadium (ppm)	2.2	15	40.0	150
Pour point (°F)	≈Zero	35	-11.0	55
Paraffin wax content (wt %)	—	3.3	—	—

* Ali, M. F et al., *Hydrocarbon Processing*, Vol. 64, No. 2, 1985 p. 83.

Pour point= The lowest temperature at which a liquid remains pourable

**TABLE IV: 2-2. TYPICAL APPROXIMATE CHARACTERISTICS AND PROPERTIES AND GASOLINE POTENTIAL OF VARIOUS CRUDES
(Representative average numbers)**

Crude source	Paraffins (% vol)	Aromatics (% vol)	Naphthenes (% vol)	Sulfur (% wt)	API gravity (approx.)	Napht. yield (% vol)	Octane no (typical)
Nigerian -Light	37	9	54	0.2	36	28	60
Saudi -Light	63	19	18	2	34	22	40
Saudi -Heavy	60	15	25	2.1	28	23	35
Venezuela -Heavy	35	12	53	2.3	30	2	60
Venezuela -Light	52	14	34	1.5	24	18	50
USA -Midcont. Sweet	-	-	-	0.4	40	-	-
USA -W. Texas Sour	46	22	32	1.9	32	33	55
North Sea -Brent	50	16	34	0.4	37	31	50

	Initial TBP range (°F)	Final TBP range (°F)
Light naphtha	60-90	180-220
Heavy naphtha	180-220	330-430
Kerosene	330-380	480-550
Light gas oil	420-520	610-650
Heavy gas oil	610-650	750-850
Vacuum gas oil	750-800	950-1,050
Vacuum residuum	950-1,050	

2.1 Distillation of crude oil

Fraction		Boiling range (°C) (at atmospheric pressure)	Number of carbon atoms in molecule	Approximat by volum
DE	→ GASES	< 20	1-4	1-2
	→ LIGHT GASOLINES OR LIGHT NAPHTHA	20-70	5-6	} 20-40
	→ NAPHTHA (MID-RANGE)	70-170	6-10	
	→ KEROSENE	170-250	10-14	10-15
	→ GAS OIL	250-340	14-19	15-20
	→ DISTILLATE FEEDSTOCKS for LUBRICATING OIL and WAXES, or HEAVY FUEL OILS	340-500	19-35	} 40-50
	→ BITUMEN	> 500 i.e. Residue	> 35	

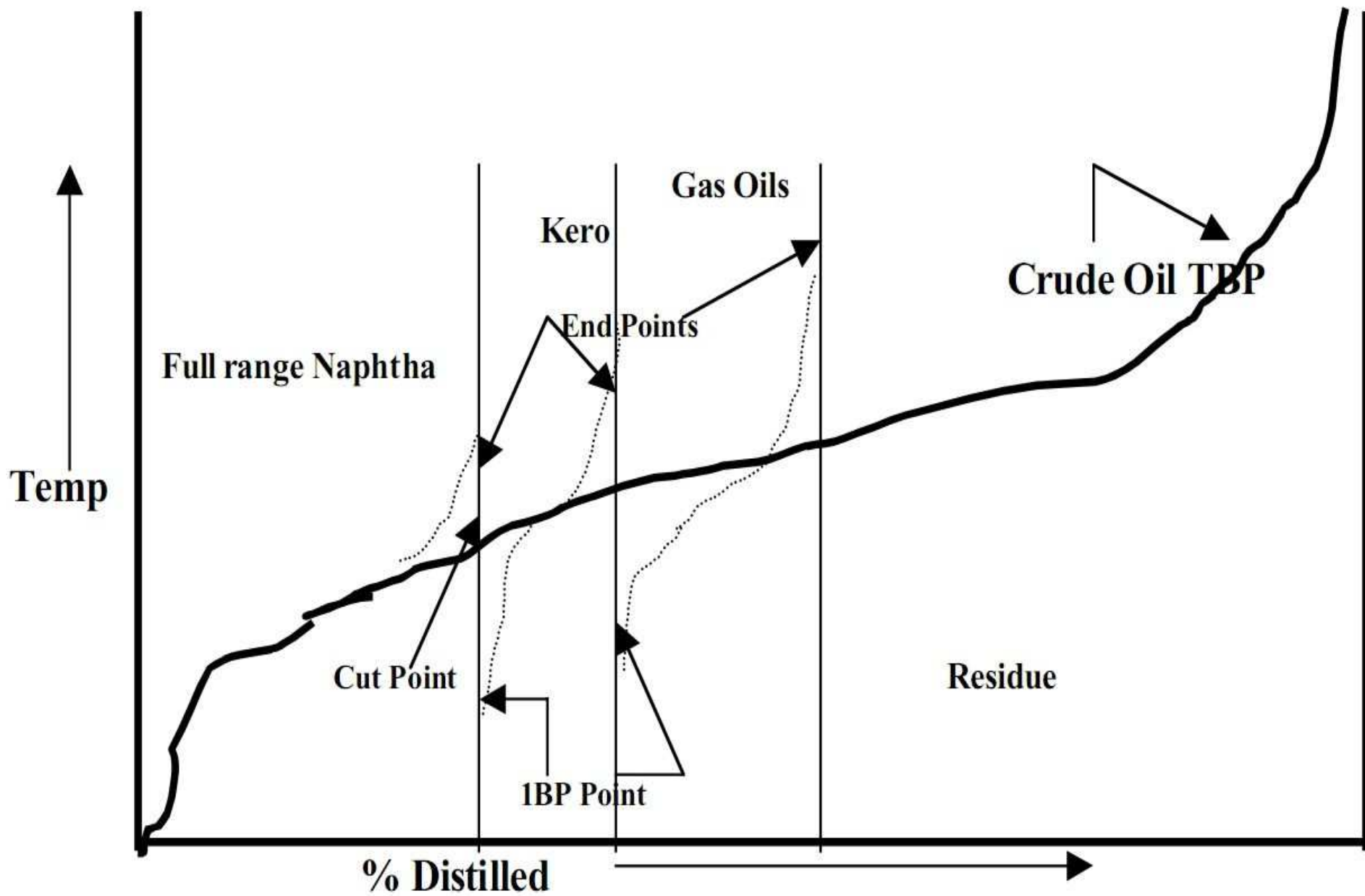


Figure 1.1. Cut points and end points.

Refinery Yield Per Barrel of Oil

Gasoline	45.8 Percent
Jet Fuel	10.7
Liquefied Gases	3.6
Kerosene	0.3
Distillate	20.9
Residual Fuel Oil	6.8
Feedstocks	2.9
Special Napthas	0.4
Lubricants	1.2
Waxes	0.1
Coke	3.9
Asphalt	3.2
Still Gas	4.8
Miscellaneous	0.5
Shortage (gain*)	-4.9

***The final total product of a refined barrel of crude oil may exceed 1 barrel, since some of the lighter liquids are in a near gaseous state and accordingly take up more volume.**

Octane numbers

Boiling points and octane ratings of different hydrocarbons in the gasoline range

Hydrocarbon	Boiling point, °F	Octane number clear	
		Research method F-1	Motor method F-2
n-Butane	0.5
n-Pentane	97	61.7	61.9
2-Methylbutane	82	92.3	90.3
2,2-Dimethylbutane	122	91.8	93.4
2,3 Dimethylbutane	137	103.5	94.3
n-Hexane	156	24.8	26.0
2-Methylpentane	146	73.4	73.5
3-Methylpentane	140	74.5	74.3
n-Heptane	208	0.0	0.0
2-Methylhexane	194	42.4	46.4
n-Octane	258	-19.0*	-15.0*
2,2,4-Trimethyl pentane (isooctane)	211	100.0	100.0
Benzene	176	...	114.8
Toluene	231	120.1	103.5
Ethylbenzene	278	107.4	97.9
Isopropylbenzene	306
o-Xylene	292	120.0*	103.0*
m-Xylene	283	145.0	124.0*
p-Xylene	281	146.0*	127.0*

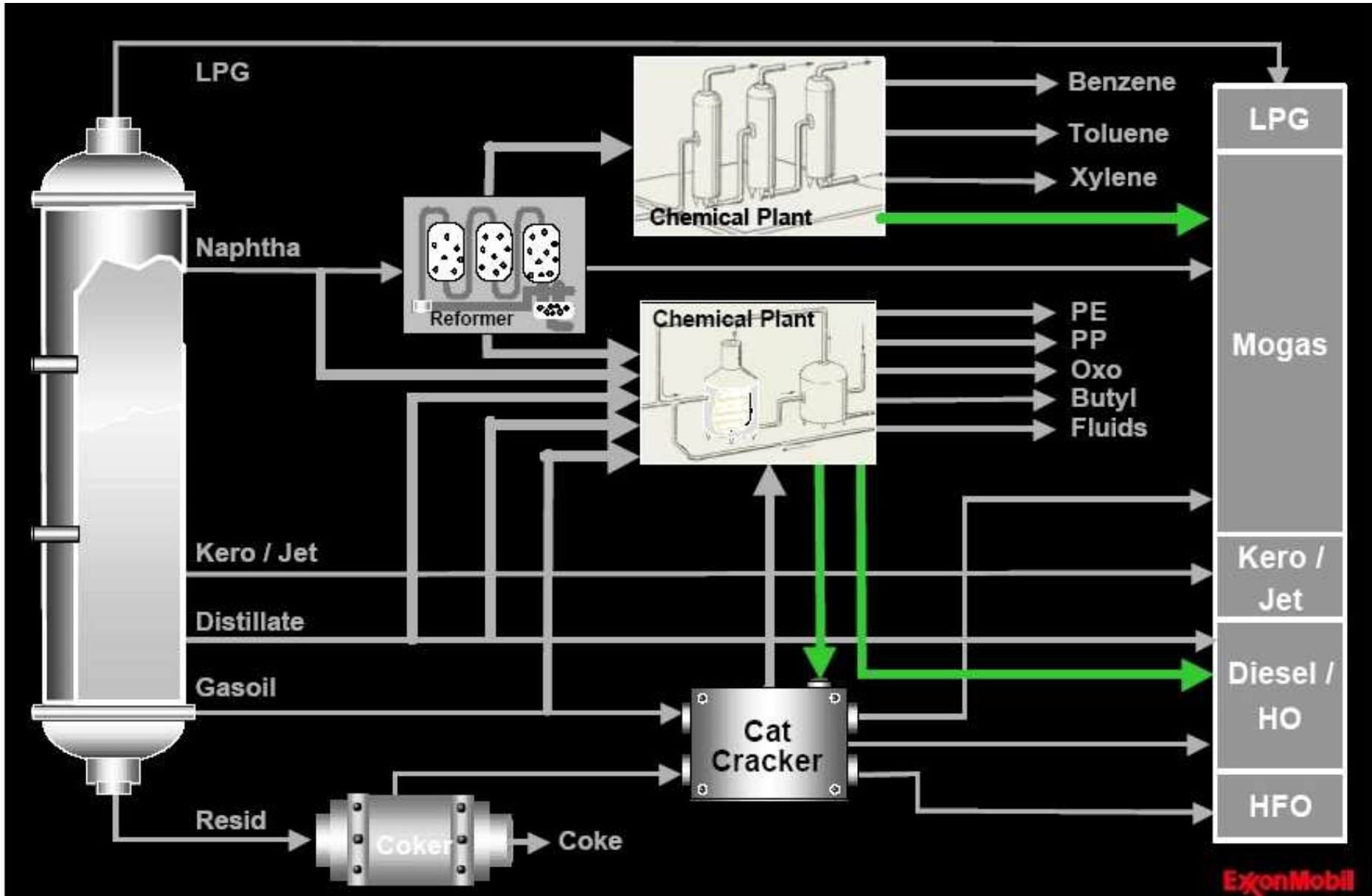
* Blending value of 20% in 60 octane number reference fuel.

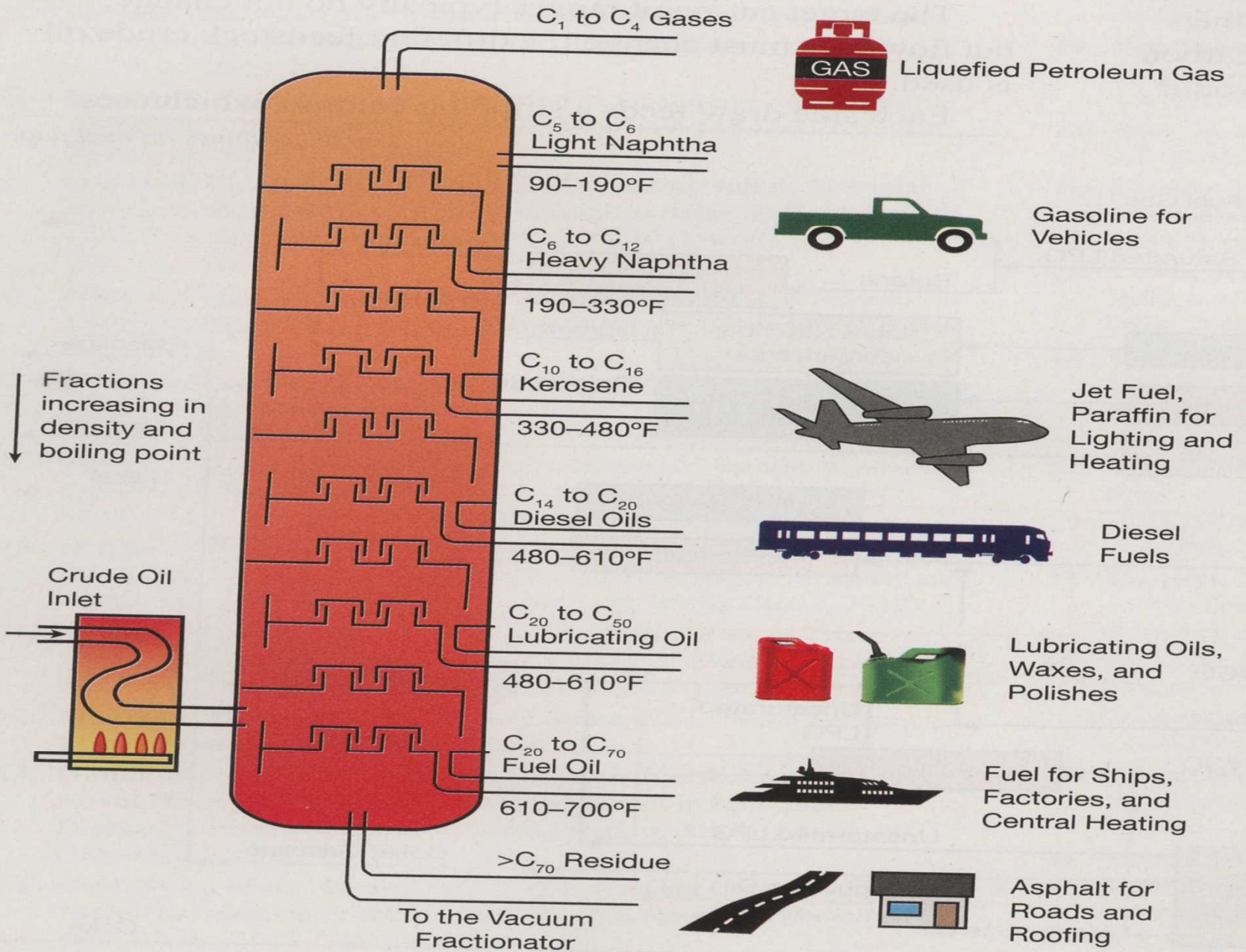
Table 2.12. Oxygenates commonly used in gasoline (subject to phase-out in the U.S.A.)

Name	Formula	RON	RVP psig	Oxygen %wt	Water solubility %*
Methyl tertiary butyl ether (MTBE)	$(\text{CH}_3)_3\text{COCH}_3$	110–112	8	18	4.3
Ethyl tertiary butyl ether (ETBE)	$(\text{CH}_3)_3\text{COC}_2\text{H}_5$	110–112	4	16	1.2
Tertiary amyl methyl ether (TAME)	$(\text{CH}_3)_2(\text{C}_2\text{H}_5)\text{COCH}_3$	103–105	4	16	1.2
Ethanol	$\text{C}_2\text{H}_5\text{OH}$	112–115	18	35	100

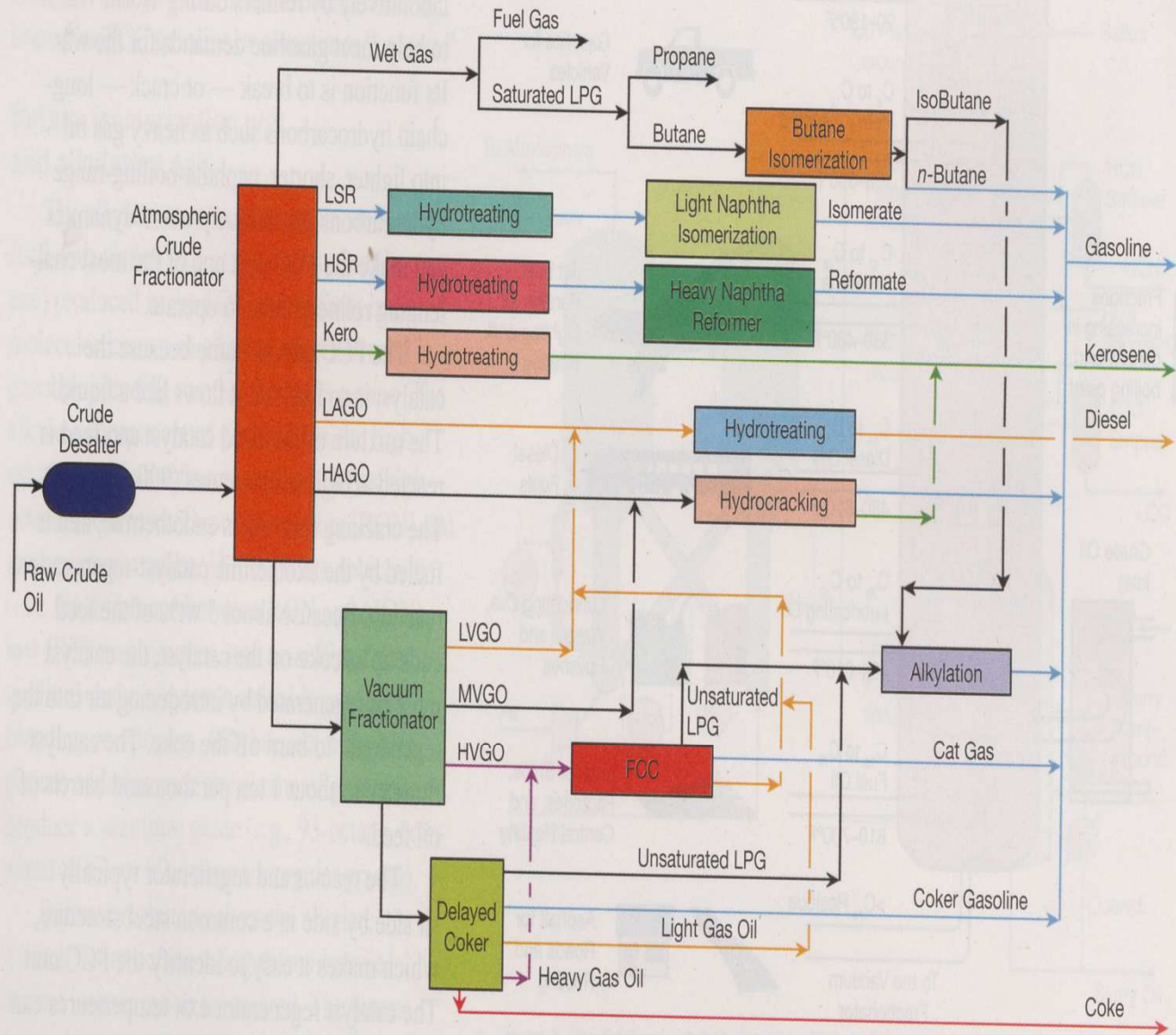
*Wt % soluble in water.

Refining

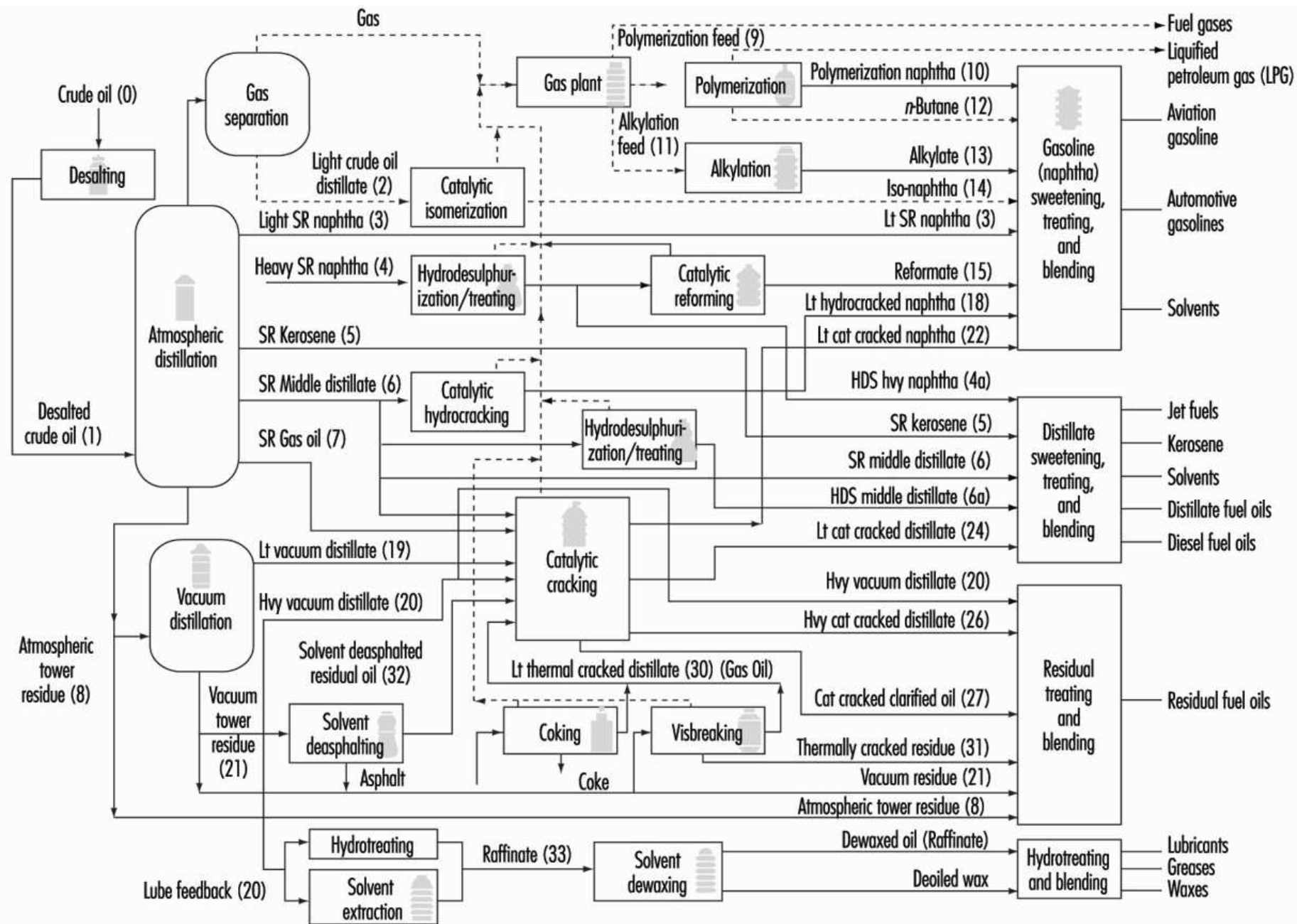




▲ **Figure 2.** One of the first major units in a refinery, the atmospheric crude fractionator



▲ **Figure 1.** This refinery flow diagram demonstrates how raw crude oil is converted into fuels. LSR = light straight-run naphtha. HSR = heavy straight run naphtha. Kero = kerosene. LAGO = light atmospheric gas oil.



Note: Numbers in parentheses refer to typical product process flow routes.

Source: OSHA 1996.

Liquids ——— Gases - - - - -

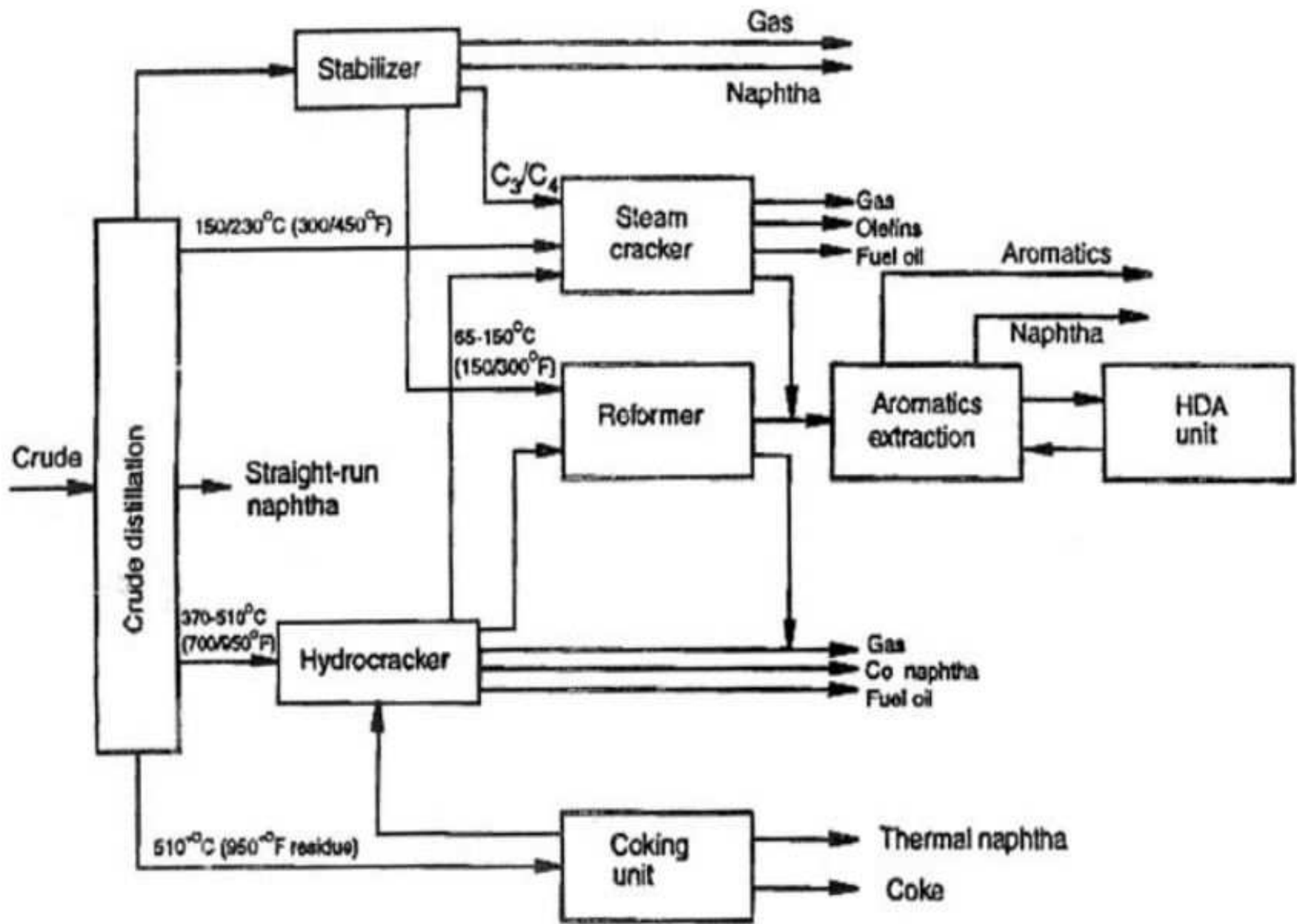
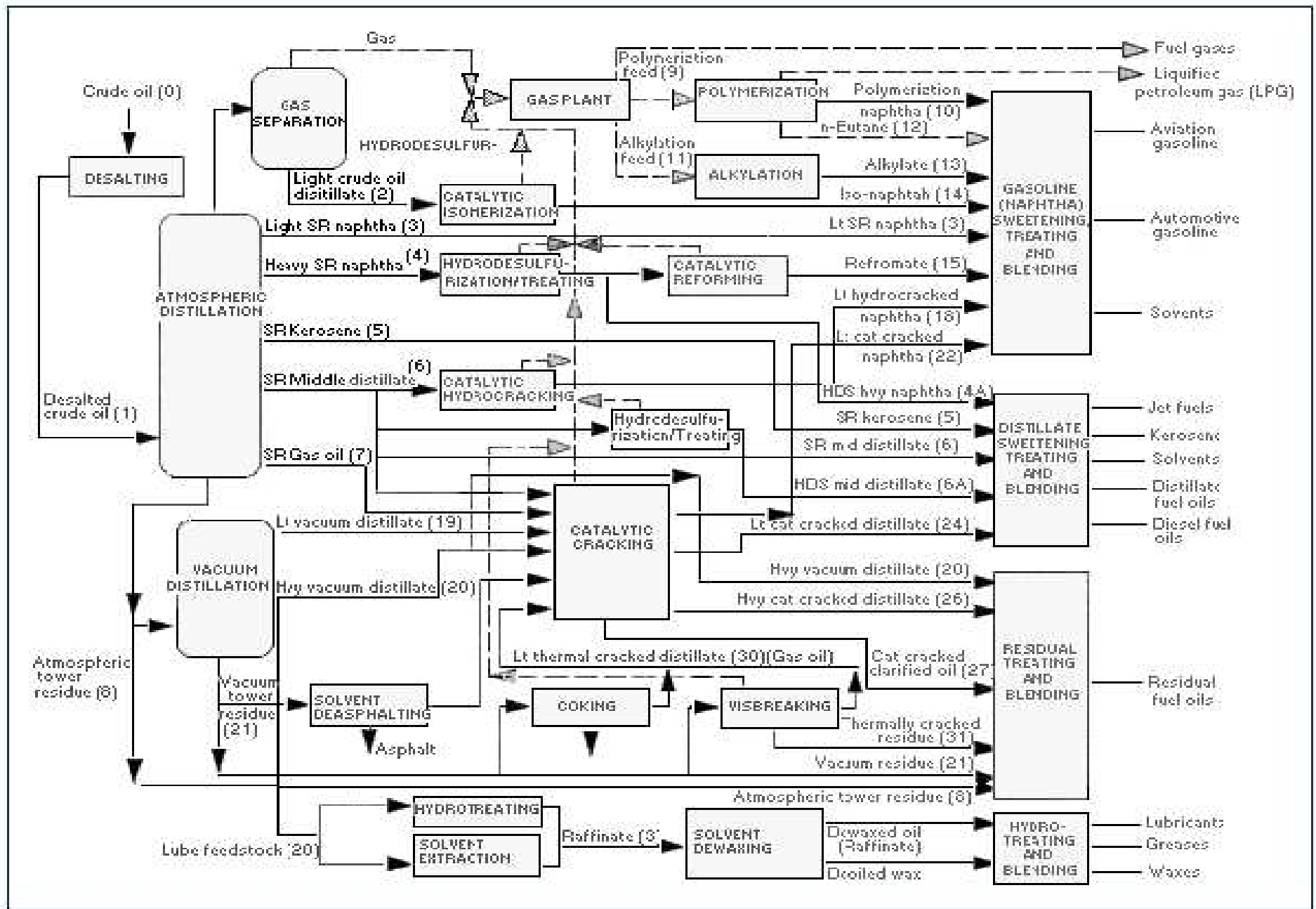


Figure 1.17. A petrochemical refinery configuration.

FIGURE IV:2-6. REFINERY PROCESS CHART.



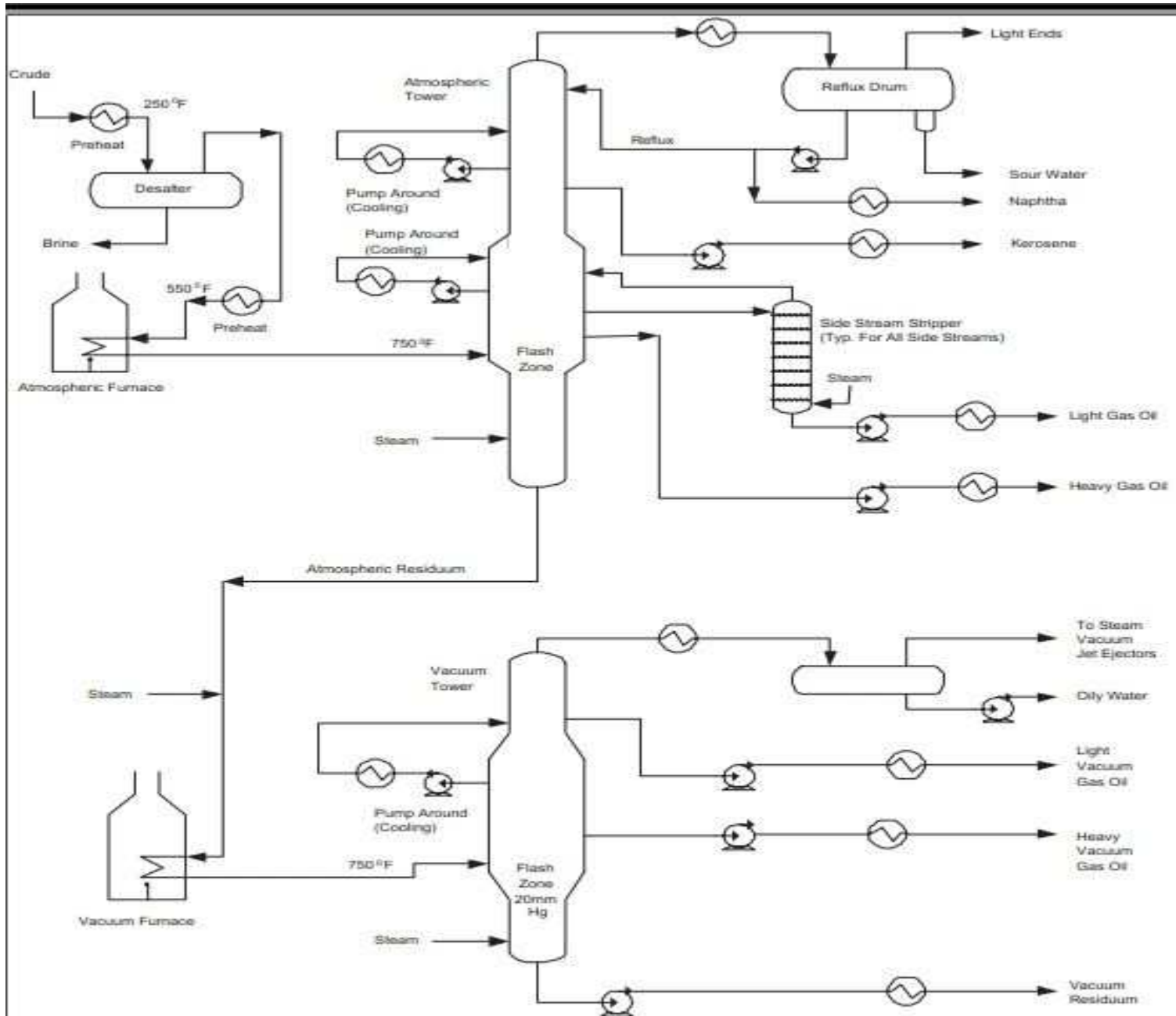


Figure 3 Crude Distillation Simplified Process Flow

Processes and Flowsheets

Process Development since the Commencement of the Modern Refining Era

Year	Process Name	Purpose	By-Products
1862	Atmospheric distillation	Produce kerosene	Naphtha, cracked residuum
1870	Vacuum distillation	Lubricants	Asphalt, residua
1913	Thermal cracking	Increase gasoline yield	Residua, fuel oil
1916	Sweetening	Reduce sulfur	Sulfur
1930	Thermal reforming	Improve octane number	Residua
1932	Hydrogenation	Remove sulfur	Sulfur
1932	Coking	Produce gasoline	Coke
1933	Solvent extraction	Improve lubricant viscosity index	Aromatics
1935	Solvent dewaxing	Improve pour point	Wax
1935	Catalytic polymerization	Improve octane number	Petrochemical feedstocks
1937	Catalytic cracking	Higher octane gasoline	Petrochemical feedstocks
1939	Visbreaking	Reduce viscosity	Increased distillate yield
1940	Alkylation	Increase octane number	High-octane aviation fuel
1940	Isomerization	Produce alkylation feedstock	Naphtha
1942	Fluid catalytic cracking	Increase gasoline yield	Petrochemical feedstocks
1950	Deasphalting	Increase cracker feedstock	Asphalt
1952	Catalytic reforming	Convert low-quality naphtha	Aromatics
1954	Hydrodesulfurization	Remove sulfur	Sulfur
1956	Inhibitor sweetening	Remove mercaptans	Disulfides and sulfur
1957	Catalytic isomerization	Convert to high-octane products	Alkylation feedstocks
1960	Hydrocracking	Improve quality and reduce sulfur	Alkylation feedstocks
1974	Catalytic dewaxing	Improve pour point	Wax
1975	Resid hydrocracking	Increase gasoline yield	Cracked residua

Process name	Action	Method	Purpose
CONVERSION PROCESSES--ALTERATION OR REARRANGEMENT			
Catalytic reforming	Alteration/ dehydration	Catalytic	Upgrade low-octane naphtha
Isomerization	Rearrange	Catalytic	Convert straight chain to branch
TREATMENT PROCESSES			
*Amine treating	Treatment	Absorption	Remove acidic contaminants
Desalting	Dehydration	Absorption	Remove contaminants
Drying & sweetening	Treatment	Abspt/ therm	Remove H ₂ O & sulfur cmpds
*Furfural extraction	Solvent extr.	Absorption	Upgrade mid distillate & lubes
Hydrodesulfurization	Treatment	Catalytic	Remove sulfur, contaminants
Hydrotreating	Hydrogenation	Catalytic	Remove impurities, saturate HC's
*Phenol extraction	Solvent extr.	Abspt/ therm	Improve visc. index, color
Solvent deasphalting	Treatment	Absorption	Remove asphalt
Solvent dewaxing	Treatment	Cool/ filter	Remove wax from lube stocks
Solvent extraction	Solvent extr.	Abspt/ precip.	Separate unsat. oils
Sweetening	Treatment	Catalytic	Remv H ₂ S, convert mercaptan

Process name	Action	Method	Purpose
CONVERSION PROCESSES--ALTERATION OR REARRANGEMENT			
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Desalting	Dehydration	Absorption	Remove contaminants
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*Furfural extraction	Solvent extr.	Absorption	Upgrade mid distillate & lubes
Hydrodesulfurization	Treatment	Catalytic	Remove sulfur, contaminants
Hydrotreating	Hydrogenation	Catalytic	Remove impurities, saturate HC's
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Solvent extraction	Solvent extr.	Abspt/ precip.	Separate unsat. oils
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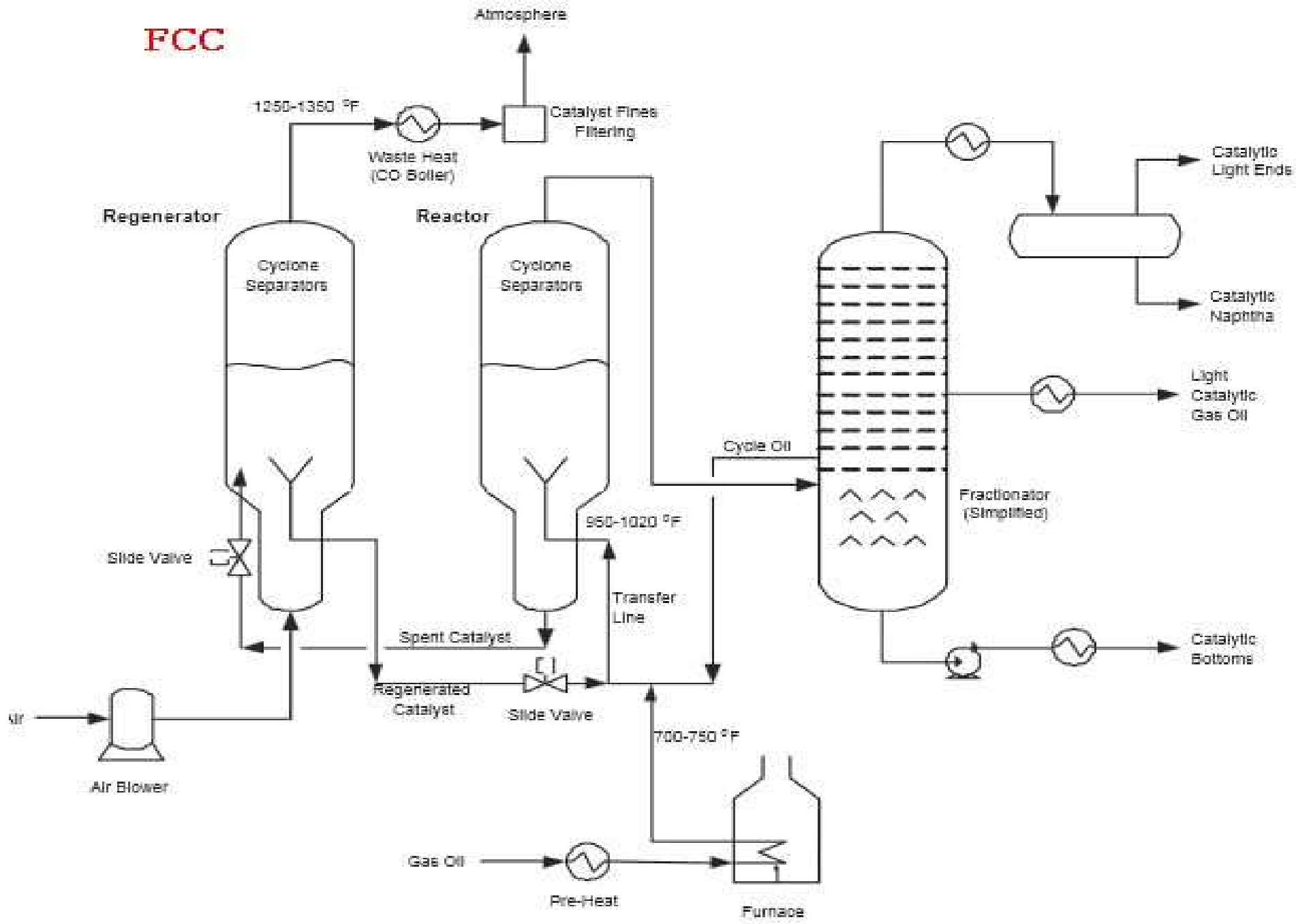
Steam cracking to olefins

Ultimate yields from steam cracking various feedstocks⁴⁵

Yield, wt %	Feedstock					
	Ethane	Propane	Butane	Naphtha	Gas oil	Saudi NGL
H ₂ + CH ₄	13	28	24	26	18	23
Ethylene	80	45	37	30	25	50
Propylene	2.4	15	18	13	14	12
Butadiene	1.4	2	2	4.5	5	2.5
Mixed butenes	1.6	1	6.4	8	6	3.5
C ₅ ⁺	1.6	9	12.6	18.5	32	9

NGL=Natural Gas Liquids

FCC



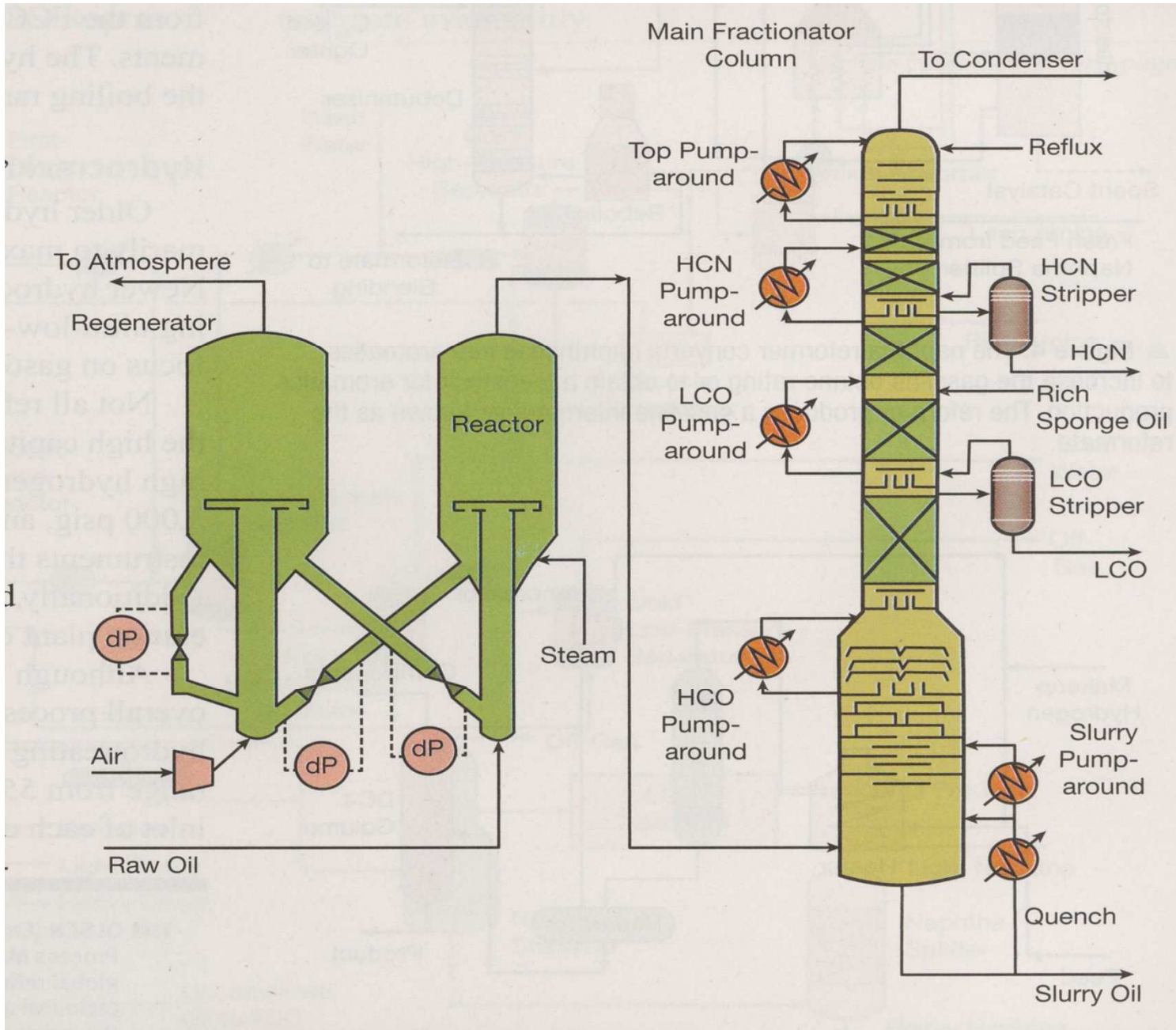
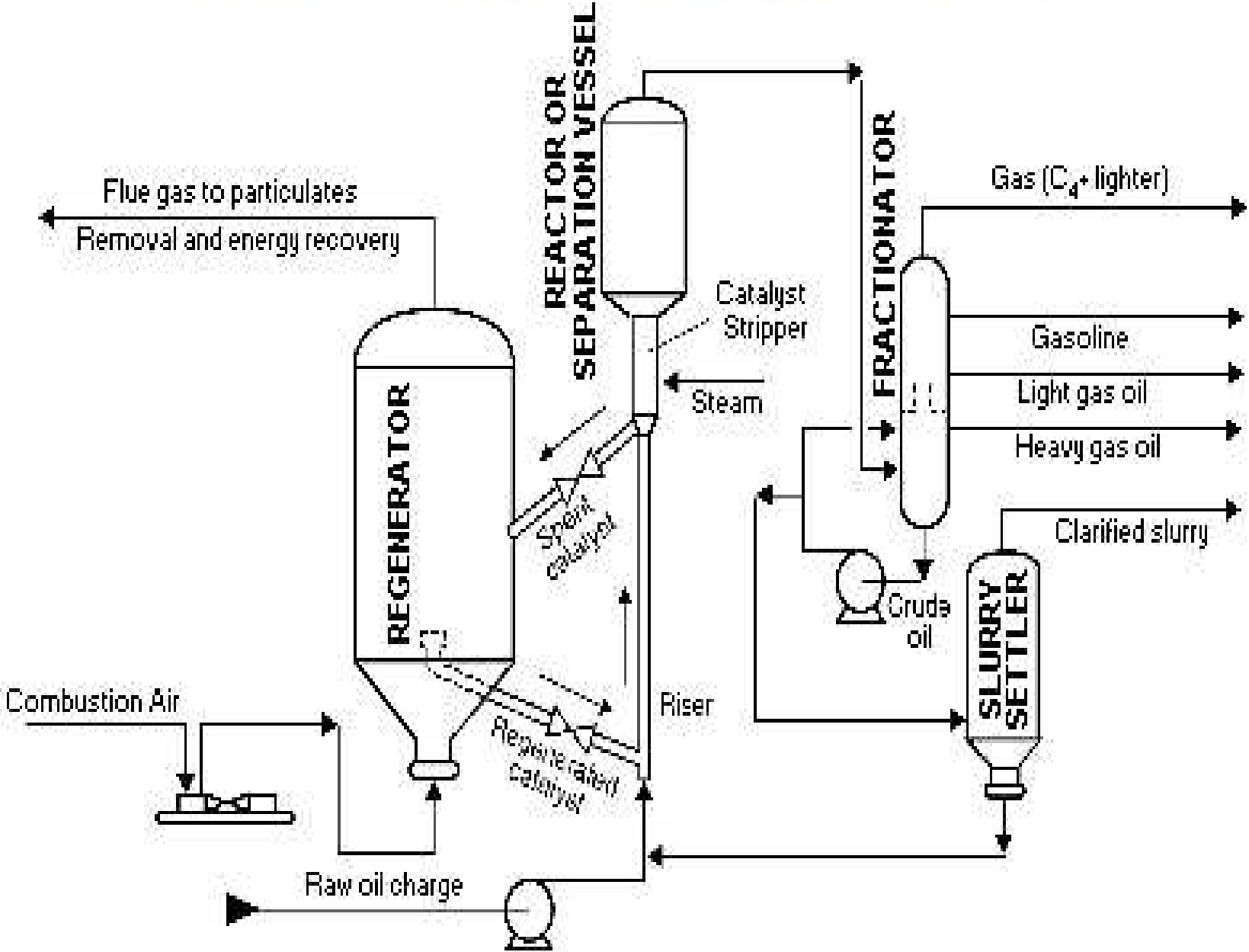


FIGURE IV:2-14. FLUID CATALYTIC CRACKING.



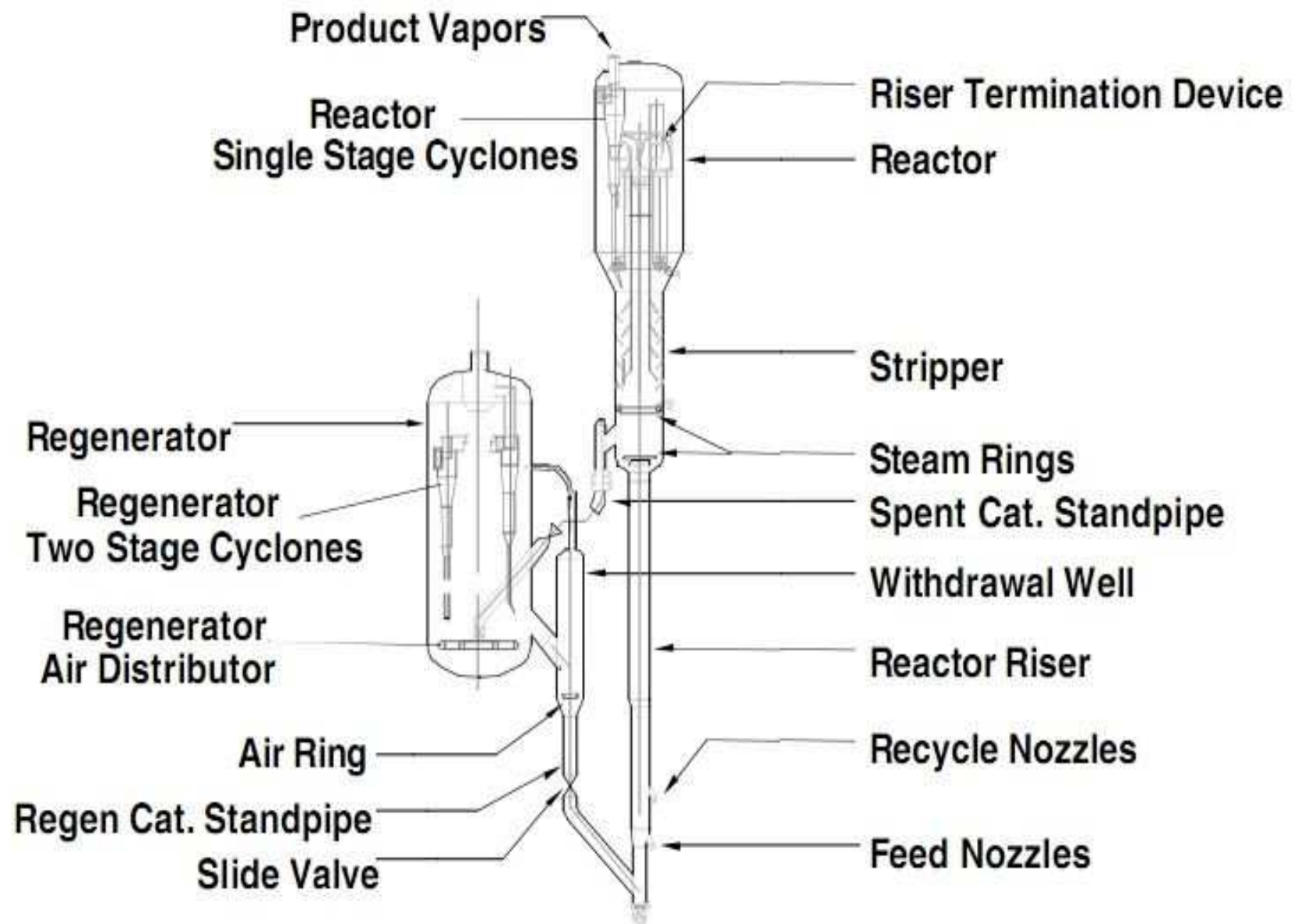
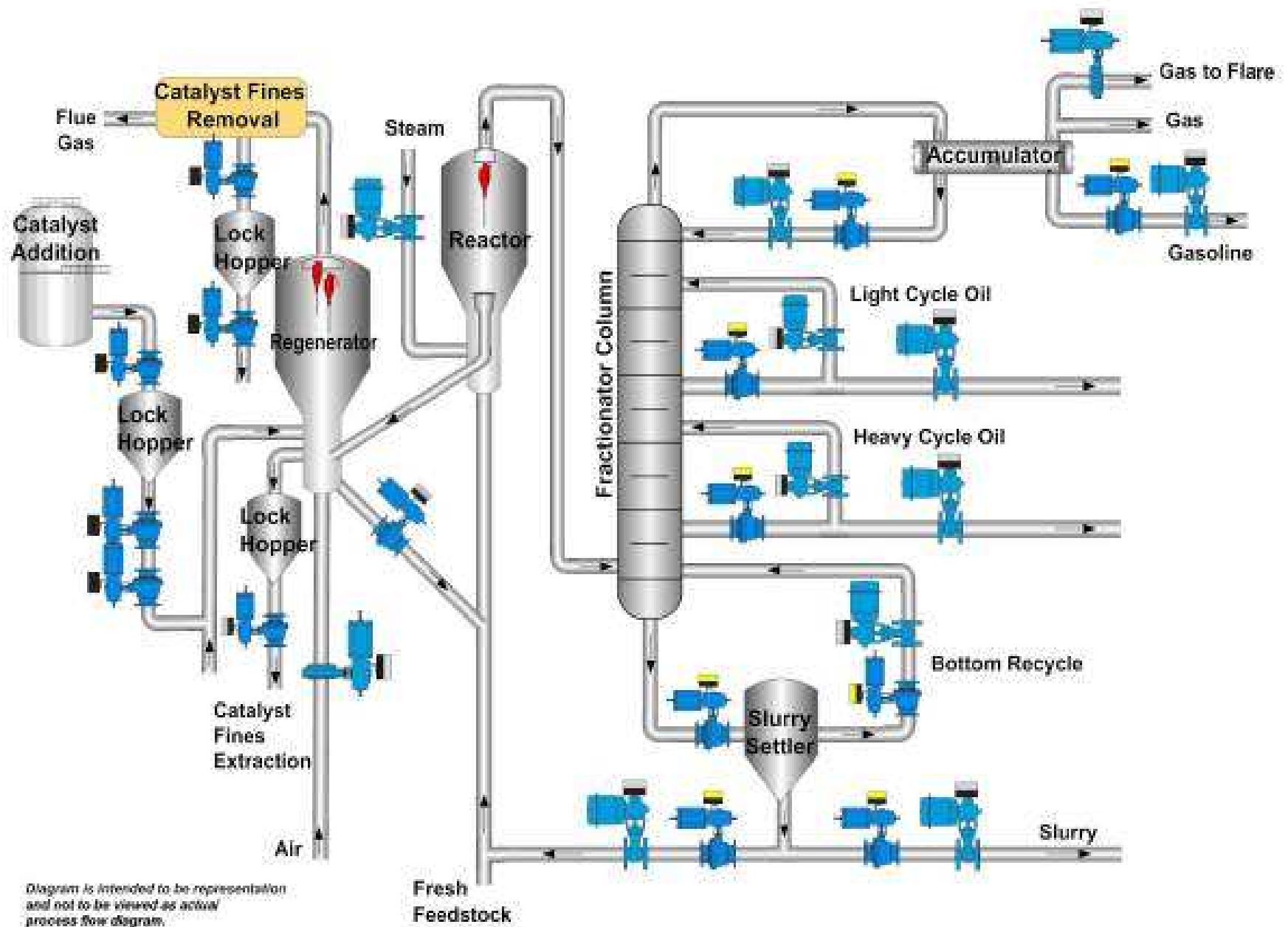
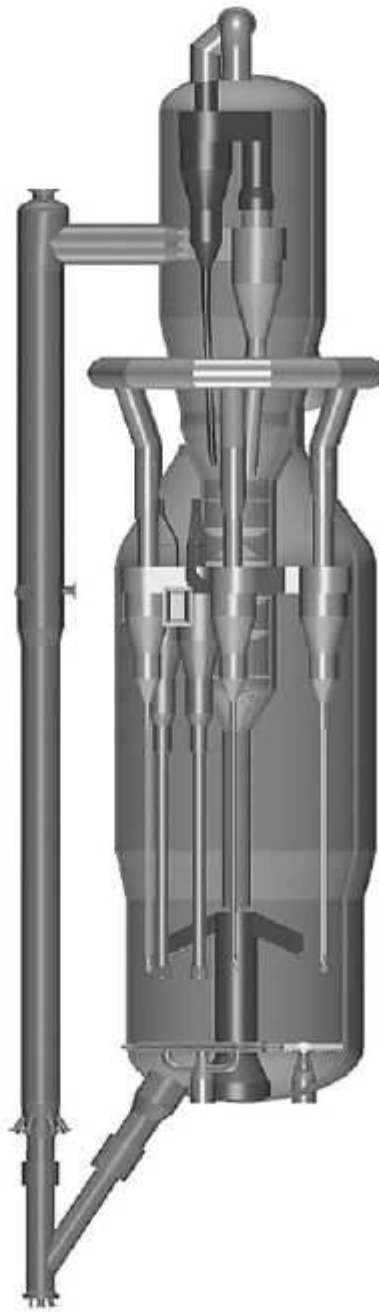


Figure 6.3. Reactor-regenerator of modern FCCU.





..... Orthoflow FCC converter.

ig valve.



..... Feed injection cone.



..... Spent catalyst stripper.

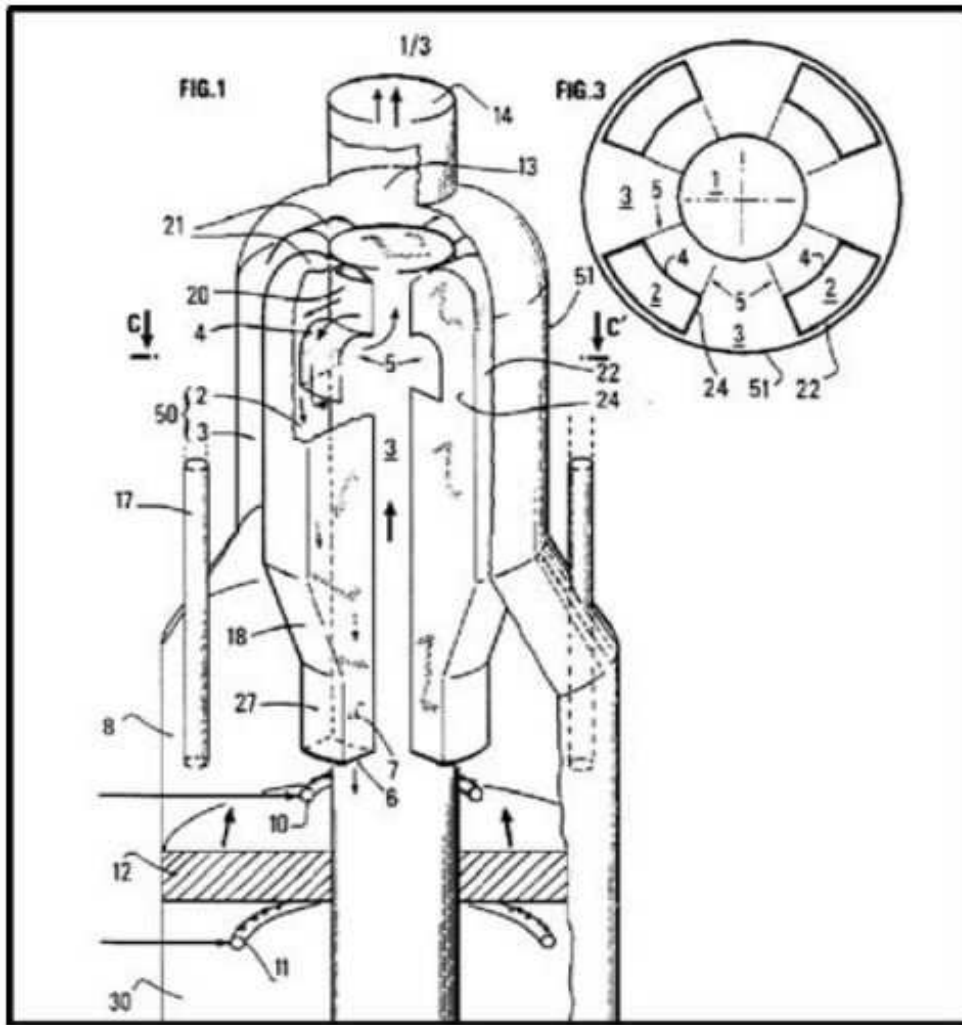


FIGURE 11.2.6 Filtering module.

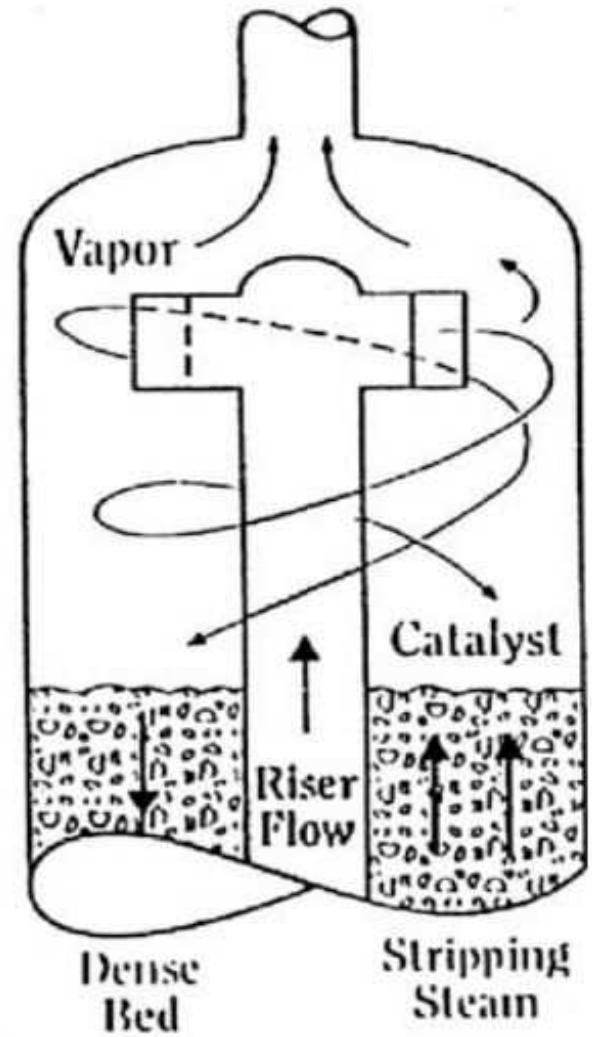


FIGURE 11.2.7 Droplet separator.

Figure 6.8. Commercial feed injection systems.



RISER SEPARATOR STRIPPER



VORTEX SEPARATOR

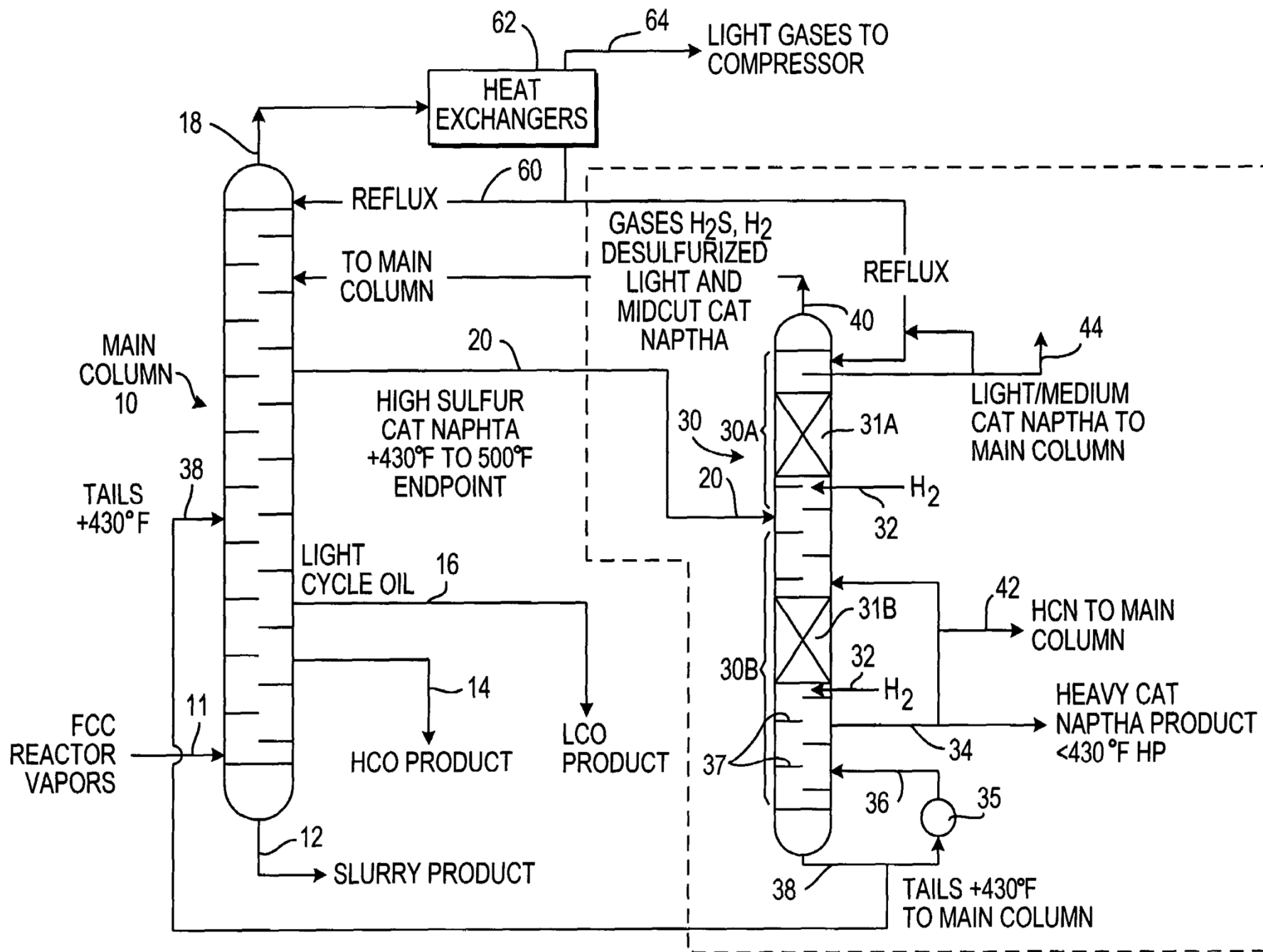
Figure 6.9. Riser separators.



FIGURE 3.4.1 SWI-IFP RFCC unit located in Japan. Photograph shows second- and first-stage regenerators and main fractionator. Note the external cyclones on the second-stage regenerator.



..... KBR Orthoflow FCC unit.



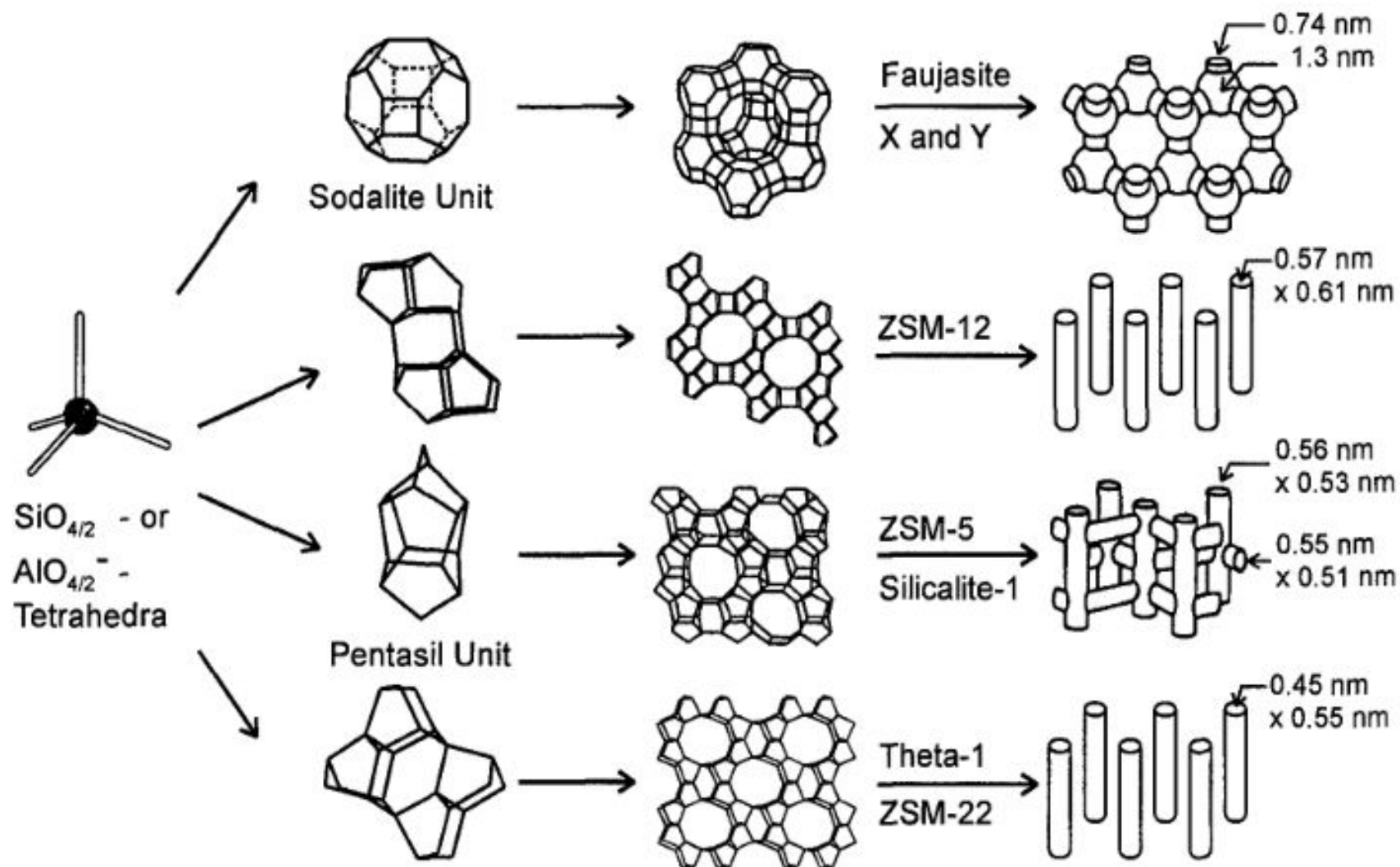


Fig. 1. Structures of four selected zeolites (from top to bottom: faujasite or zeolites X, Y; zeolite ZSM-12; zeolite ZSM-5 or silicalite-1; zeolite Theta-1 or ZSM-22) and their micropore systems and dimensions.

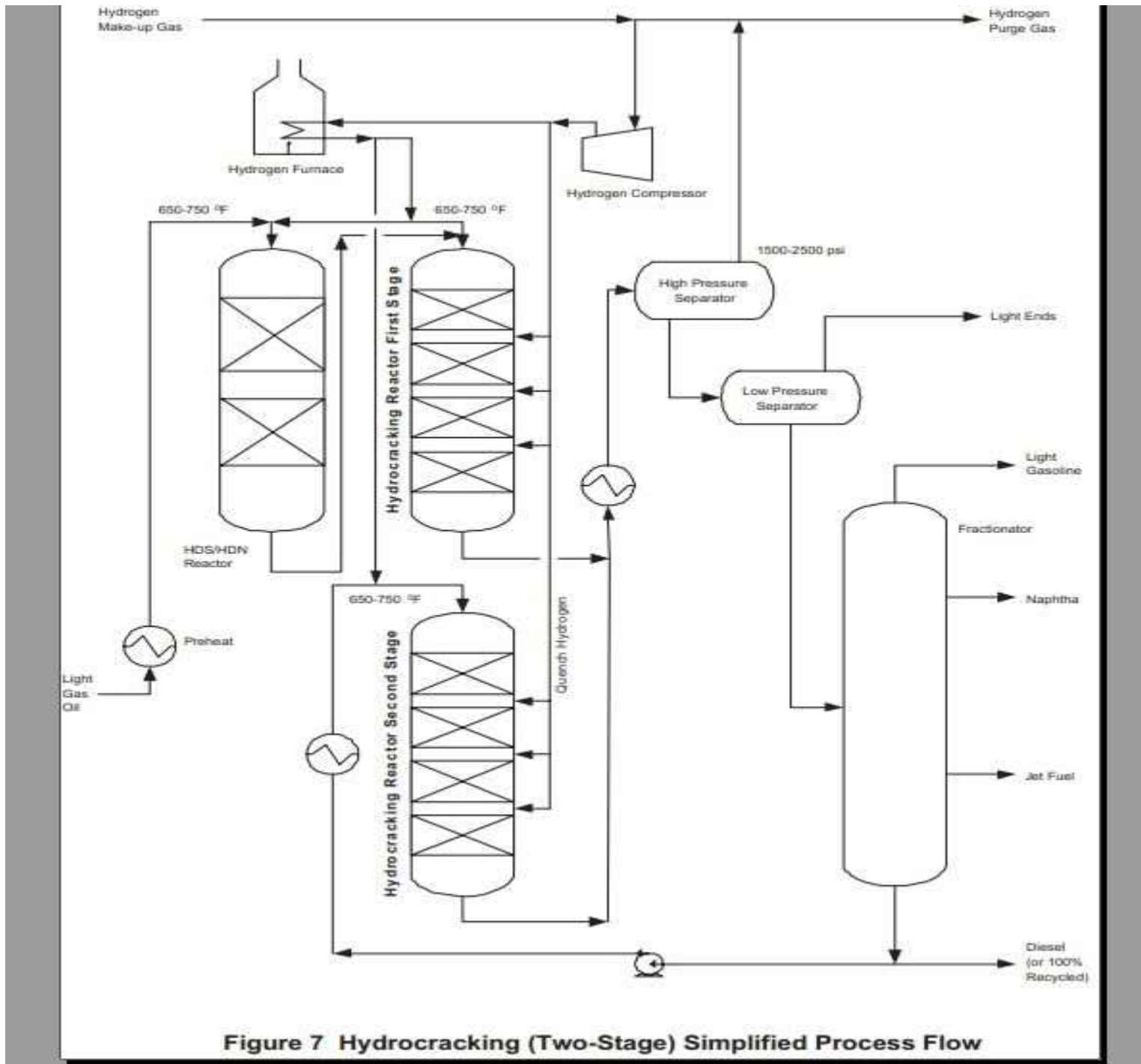
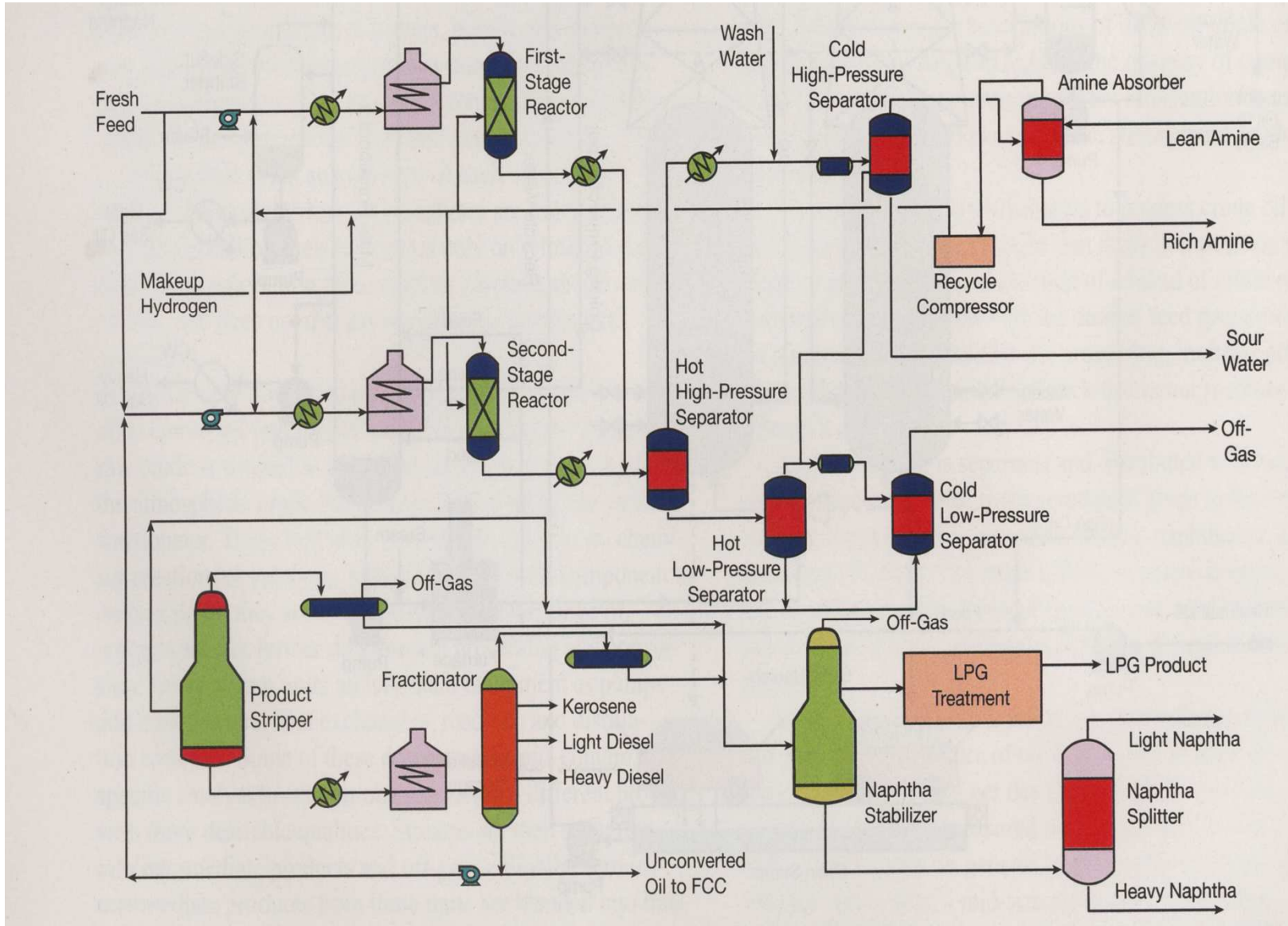
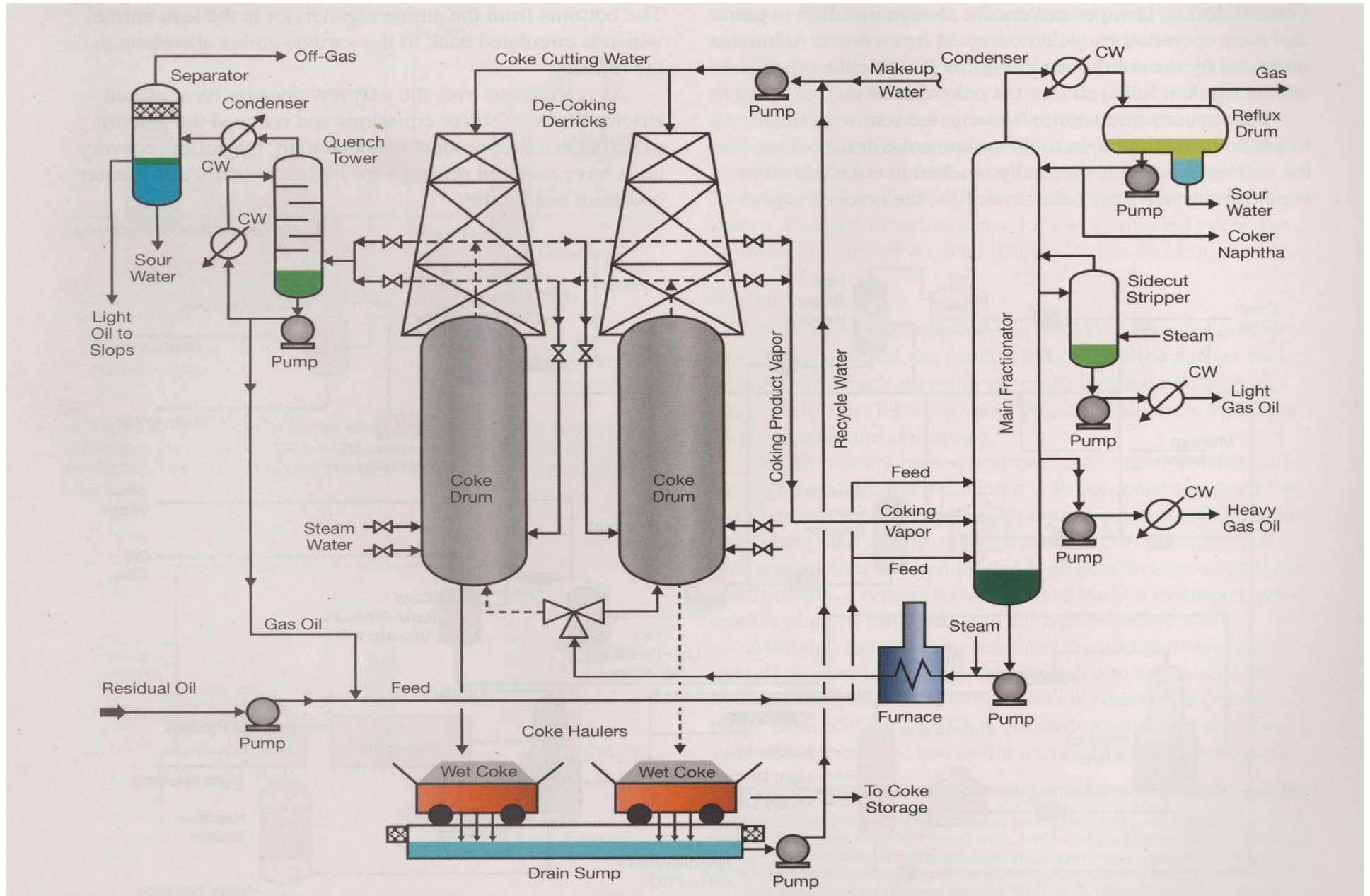


Figure 7 Hydrocracking (Two-Stage) Simplified Process Flow

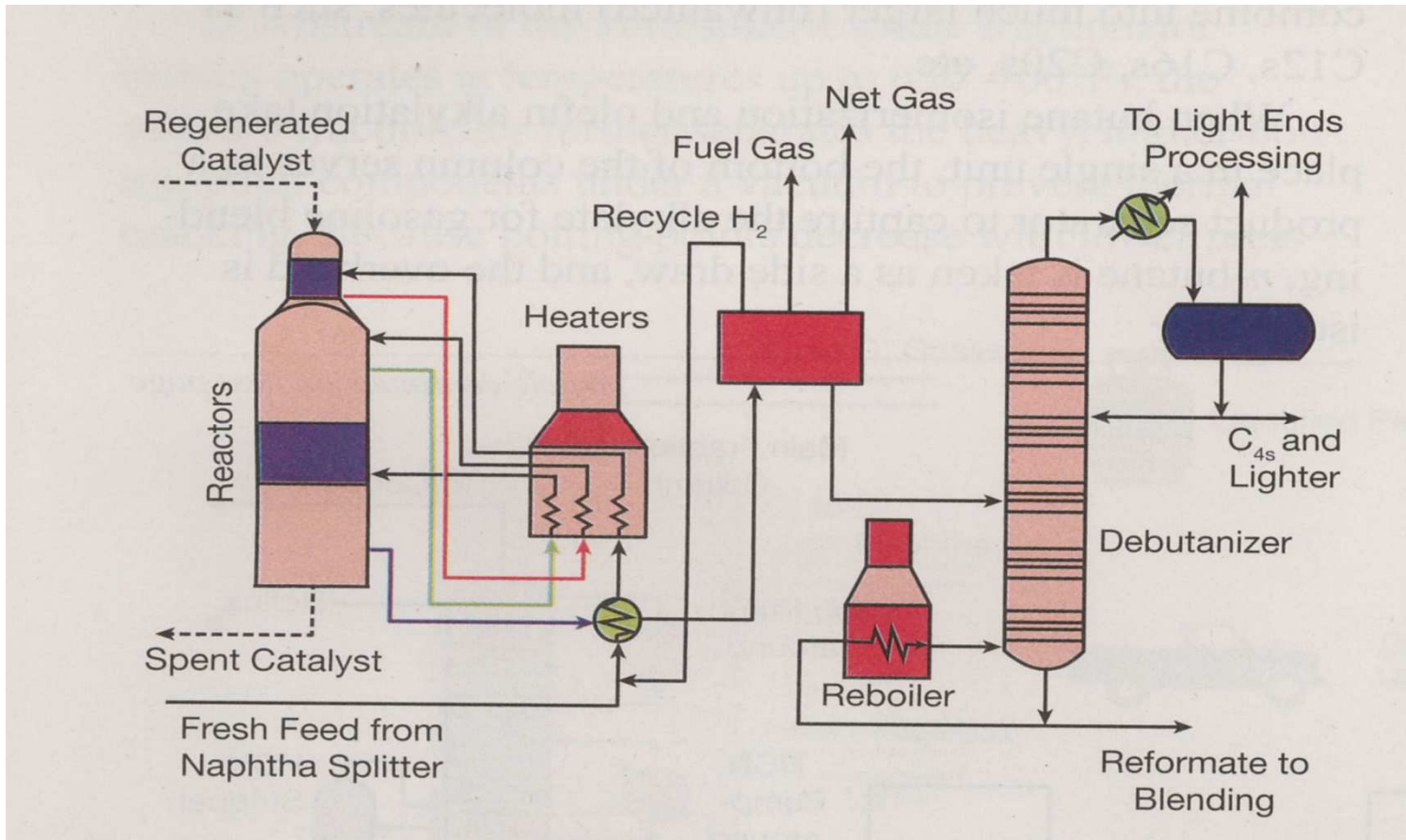
Hydrocracking



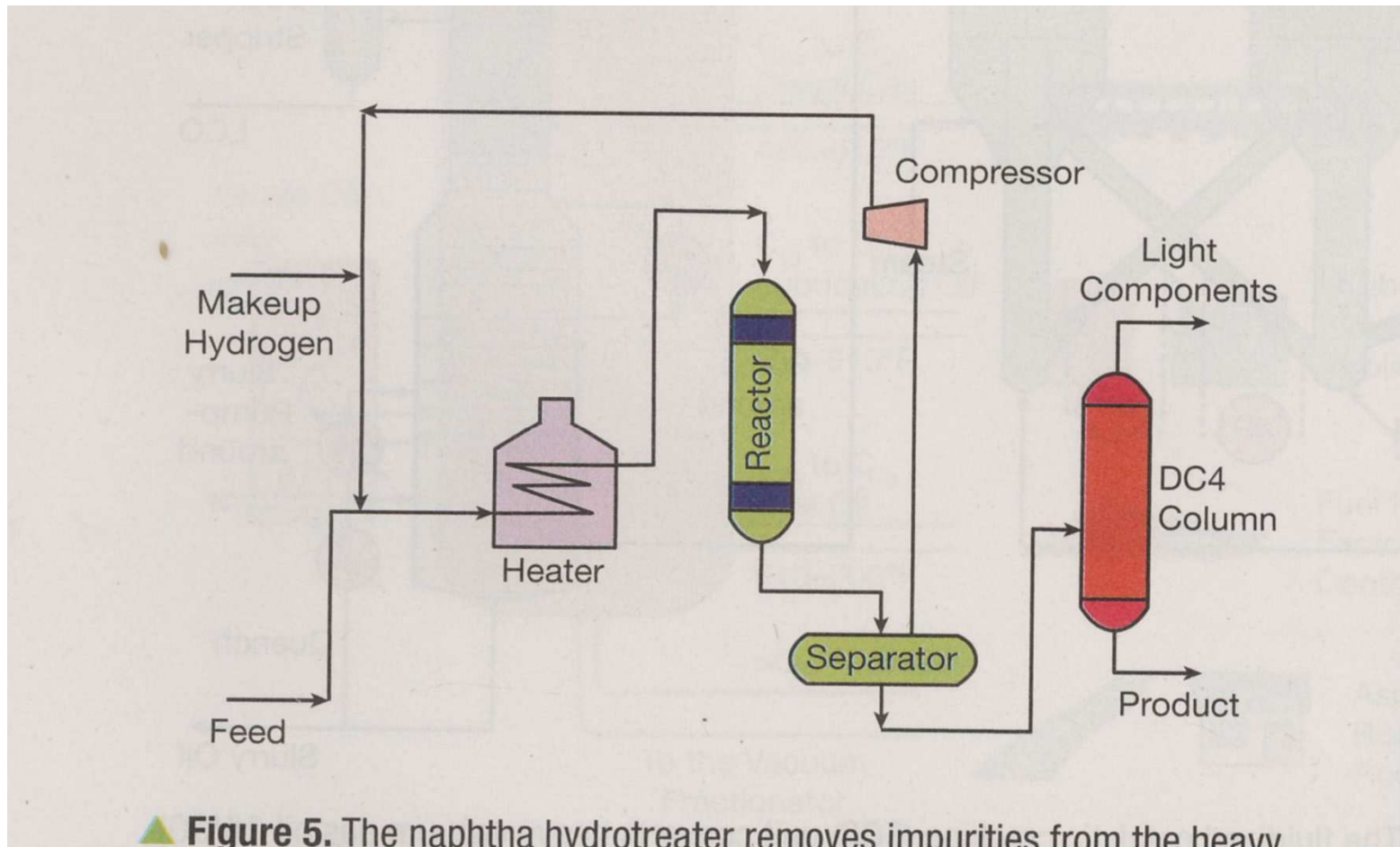
Delayed coking



Naphta reformer



Naphta hydrotreater



▲ **Figure 5.** The naphtha hydrotreater removes impurities from the heavv

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אין יבוא ואין תחרות

בית הזיקוק בחיפה מחזיק בתואר "בית הזיקוק הגדול במזרח התיכון". הוא בעל יכולת זיקוק של 197 אלף חביות נפט ביממה, פי שניים מבית הזיקוק באשדוד.

הנפט הגולמי מגיע לבית הזיקוק בטמפרטורת הסביבה. תהליך הזיקוק שלו כולל את חימום הנפט ועיבוי ברמות טמפרטורות שונות, שנעשה באמצעות כבשני ענק שעל דפנותיהם צינורות שבהם זורם הנפט המחומם. החימום לרמות של מאות מעלות צלזיוס מאפשר את הפרדת חומריו השונים של הנפט על סמך נקודת הרתיחה של כל חומר המרכיב אותו.

מגדלי הזיקוק נדרשים להיות גבוהים, מכיוון שהאדים עולים מעלה. לאחר תהליך האידוי והעיבוי, שלב הזיקוק הבא הוא הפיצוח, שבמהלכו משתמשים בזרזים הנמצאים גם בקנקני סינון המים בריטה ומתקני טיהור אחרים, המזקקים את הנפט ברמה אחת נוספת. במקביל מבצעים "הדחה" – שטיפה של הנפט – המזקקת אותו עוד יותר.

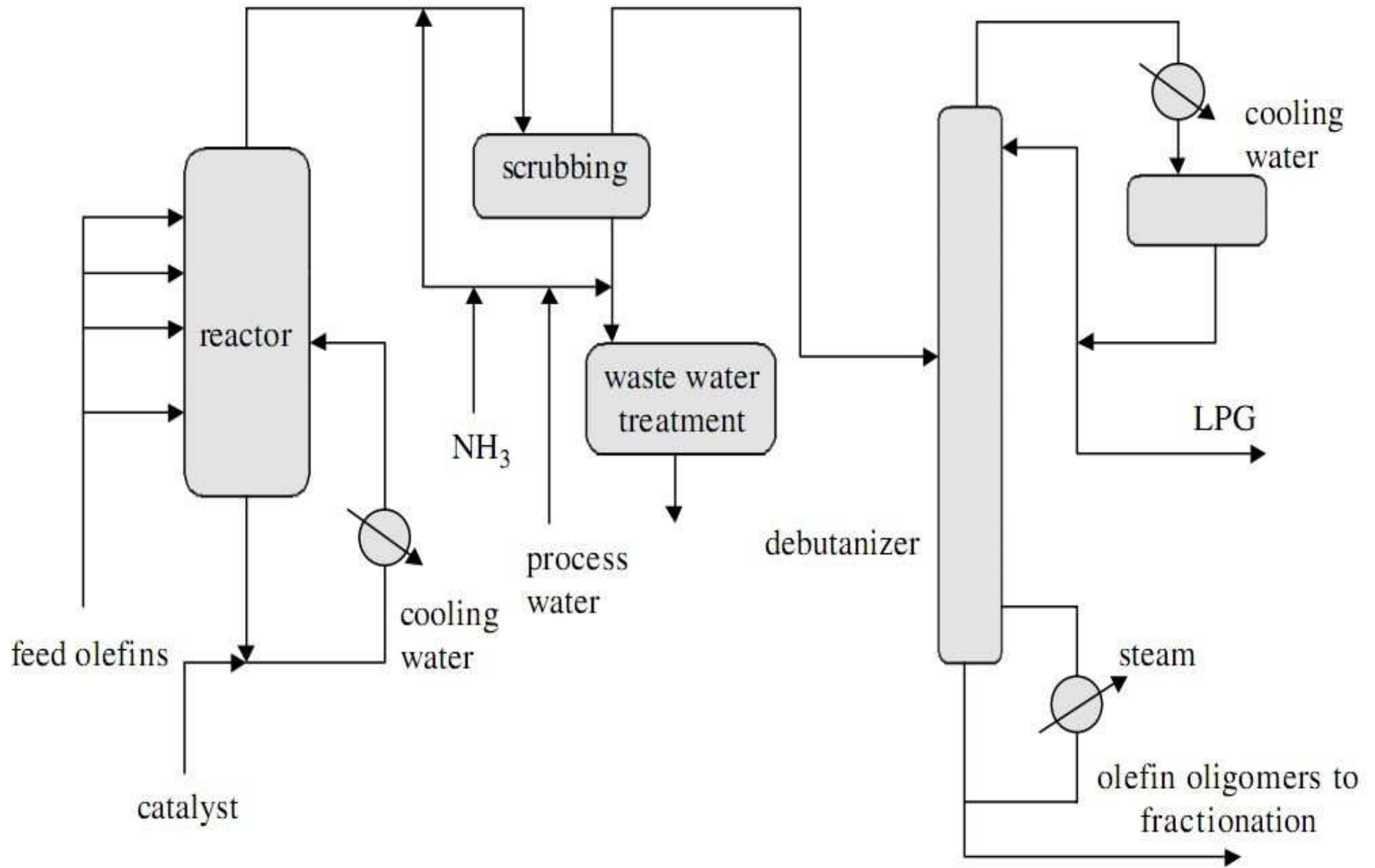
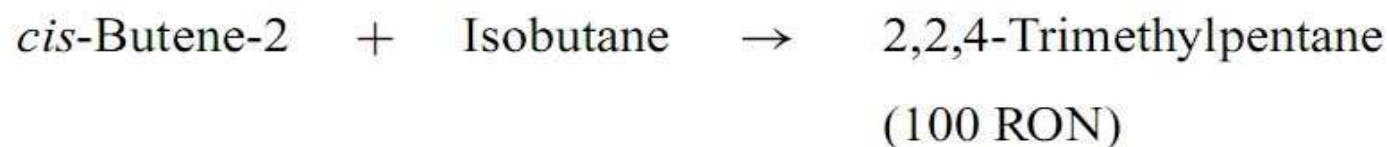
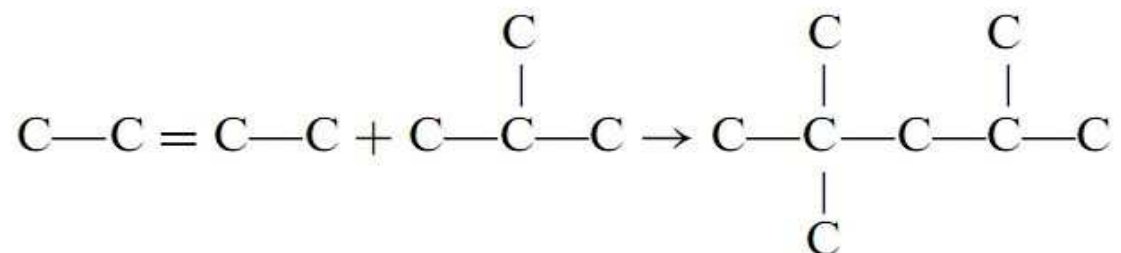
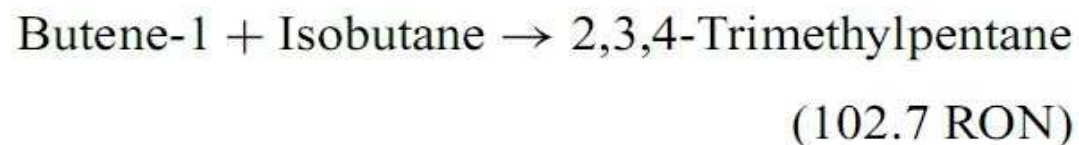
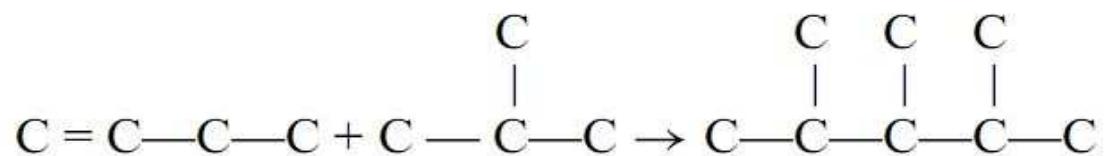
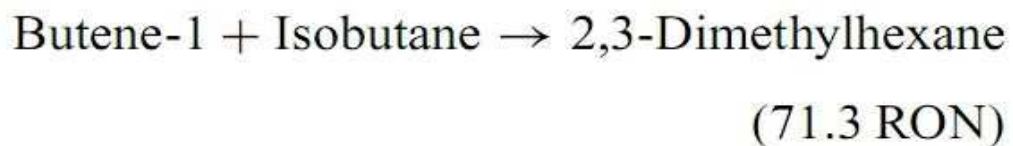


Figure 9.2.7. Dimersol process (IFP).

ALKYLATION OF BUTENE-2



ALKYLATION OF BUTENE-1



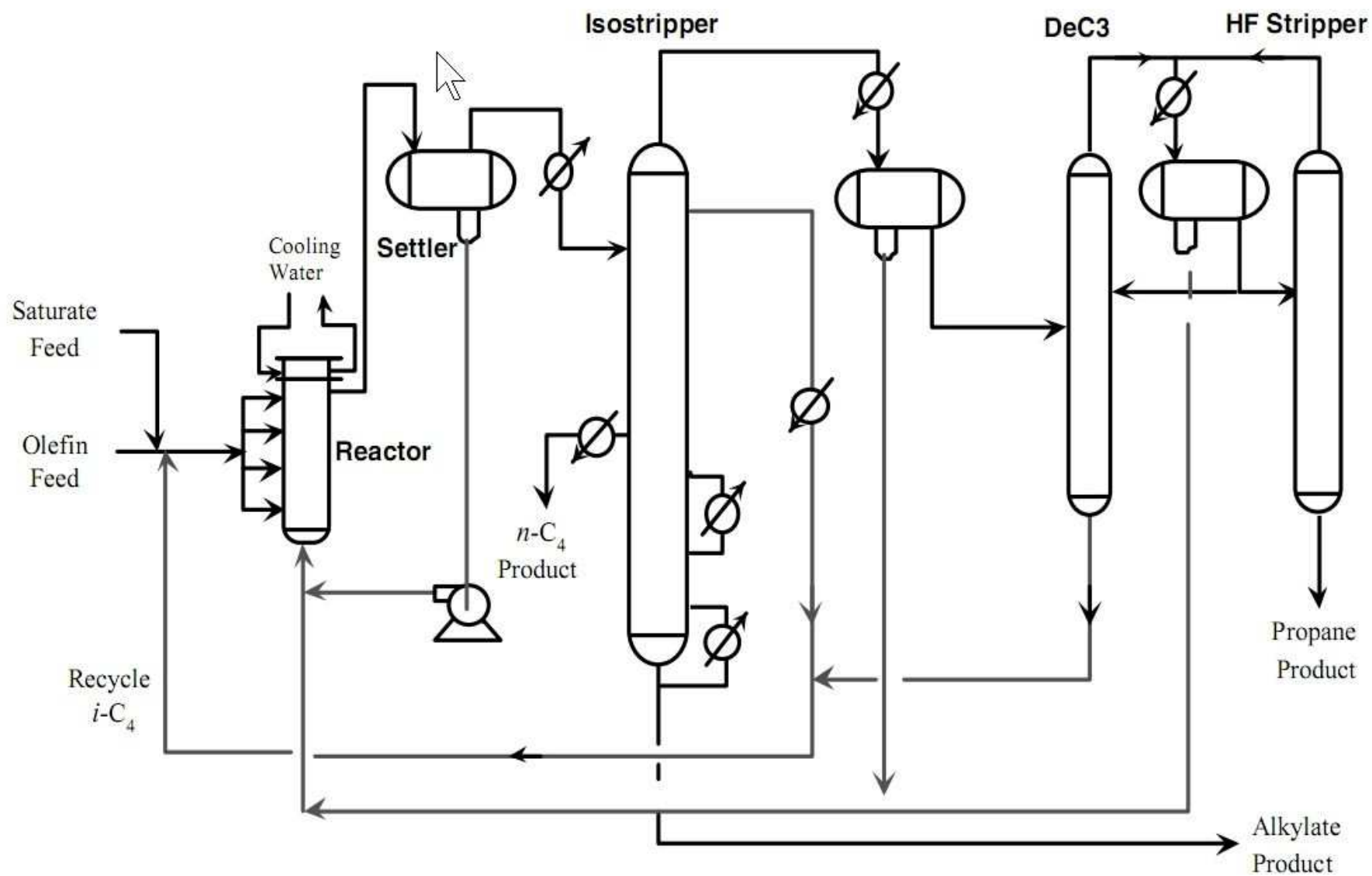


Figure 9.1.2. UOP HF alkylation.

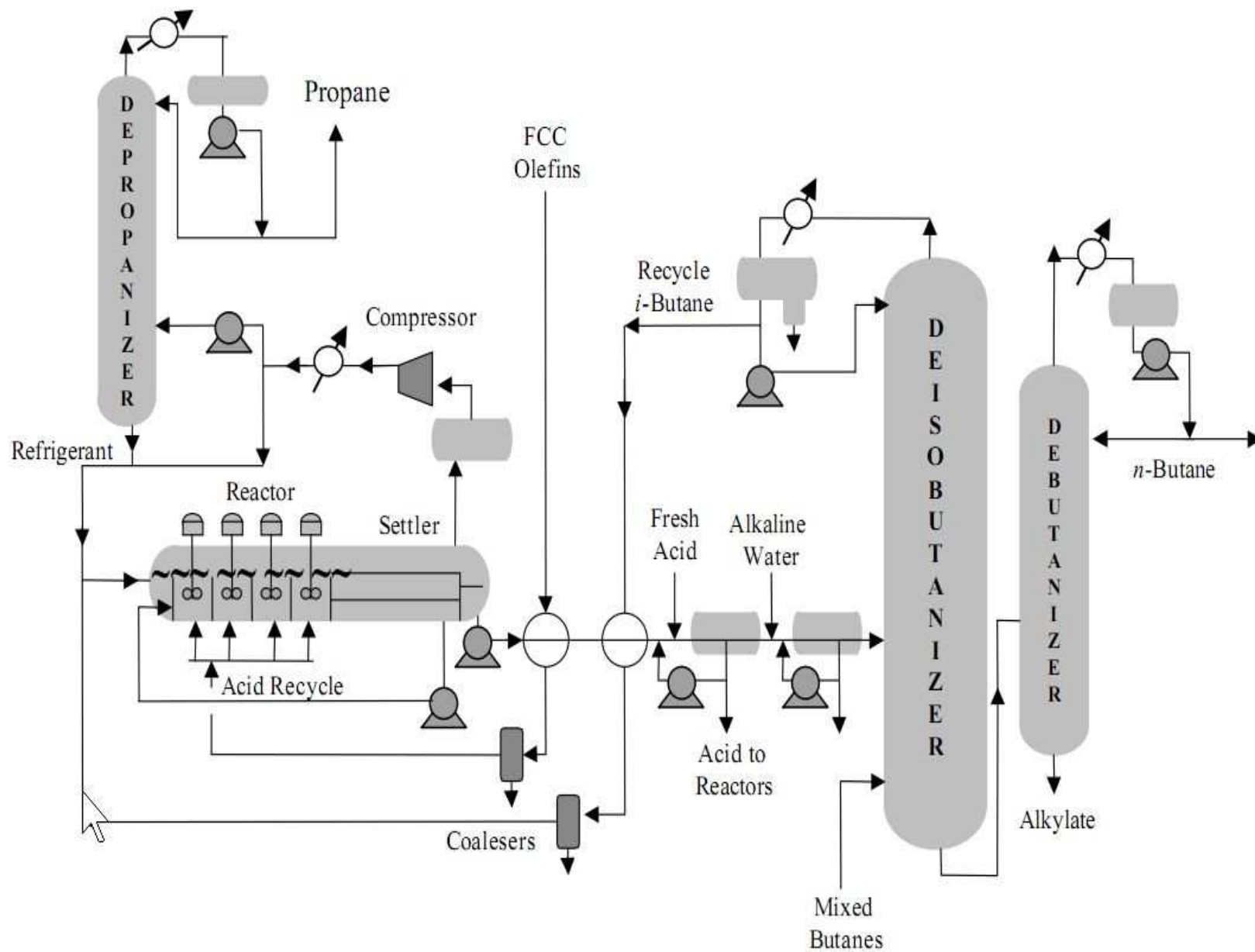
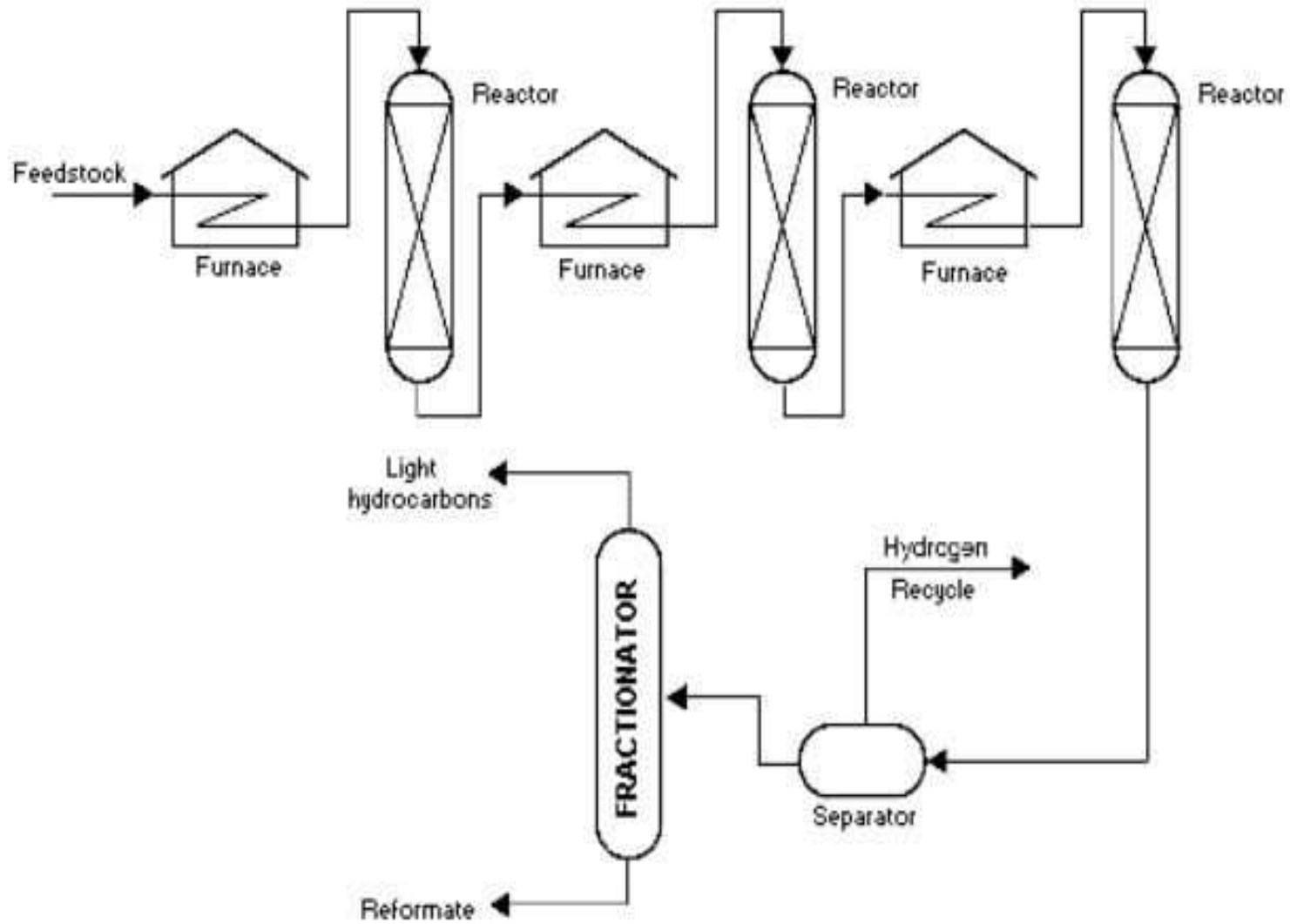
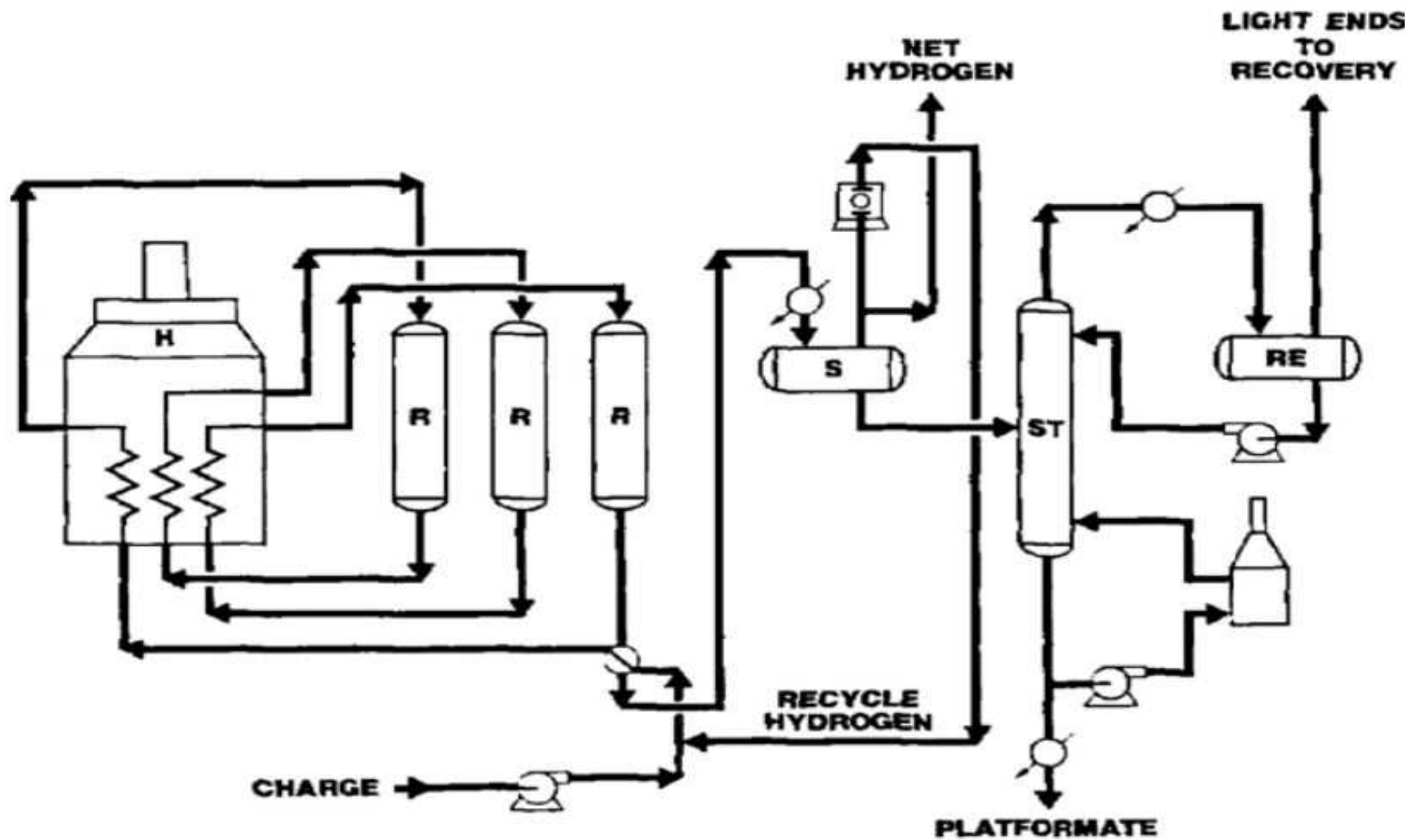


Figure 9.1.3. Cascade auto-refrigerated alkylation process.

FIGURE IV:2-16. PLATFORMING PROCESS.



UOP PLATFORMING PROCESS

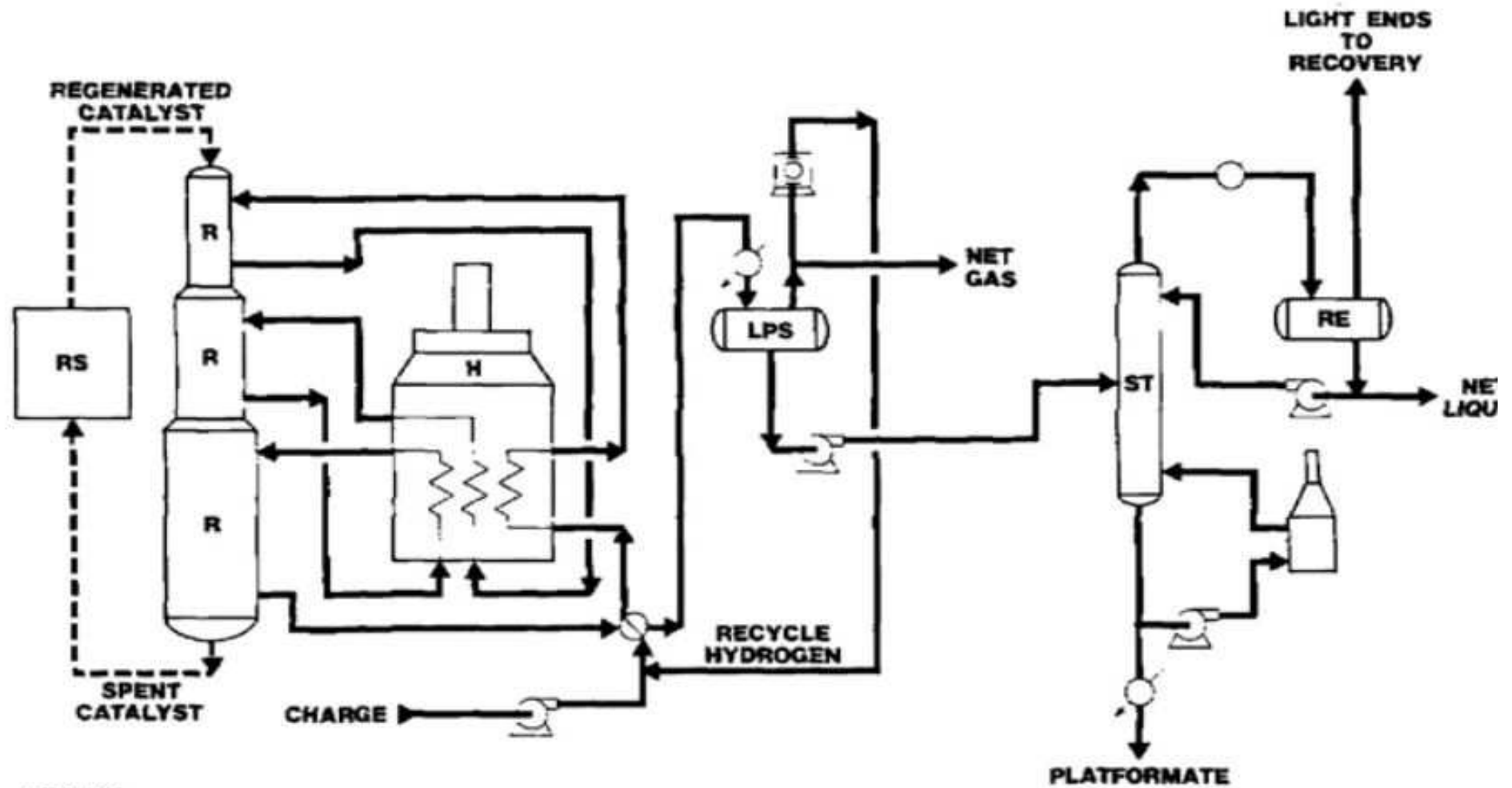


LEGEND

H = HEATER
R = REACTOR
RE = RECEIVER
S = SEPARATOR
ST = STABILIZER

Figure 5.6. Semiregenerative reforming process (reprinted with permission from UOP LLC).

UOP CONTINUOUS PLATFORMING PROCESS



LEGEND

- | | |
|------------------------------|---------------------------|
| C - CHILLER | RE - RECEIVER |
| H - HEATER | RS - REGENERATION SECTION |
| LPS - LOW PRESSURE SEPARATOR | ST - STABILIZER |
| R - REACTOR | |

Figure 5.7. CCR Platforming process (reprinted with permission from UOP LLC).

Desulfurisation

Sulfur treatment of gas fractions

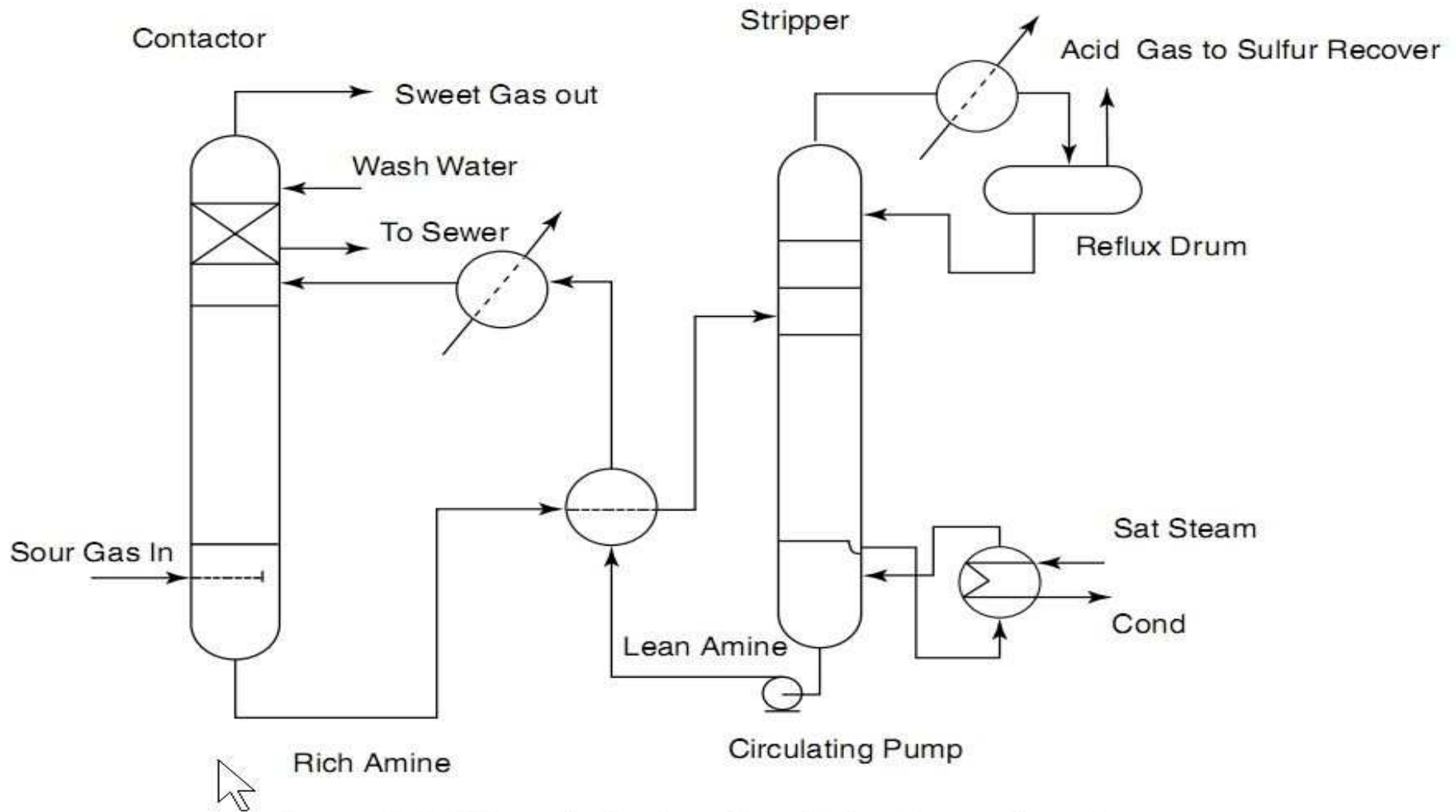
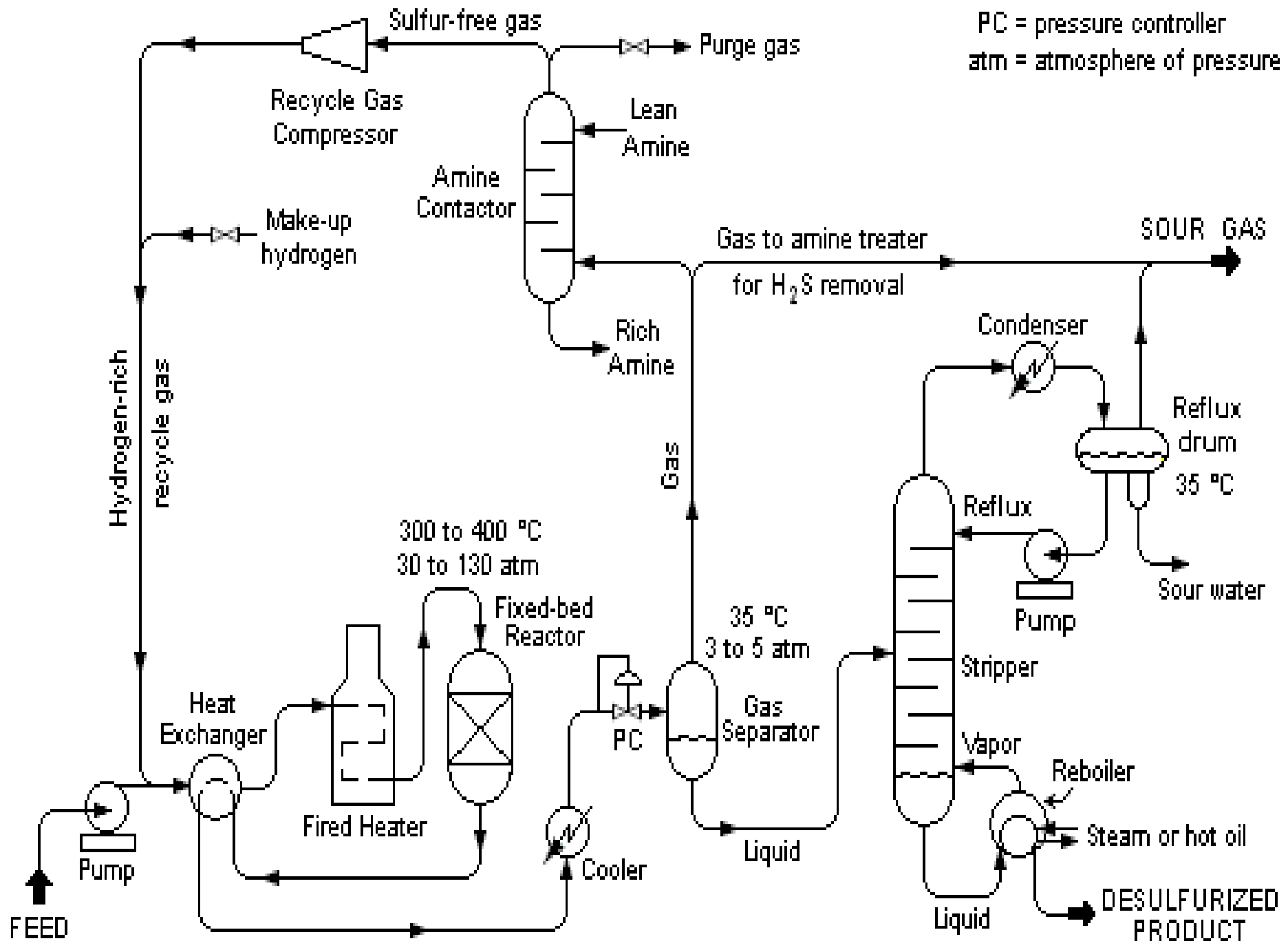


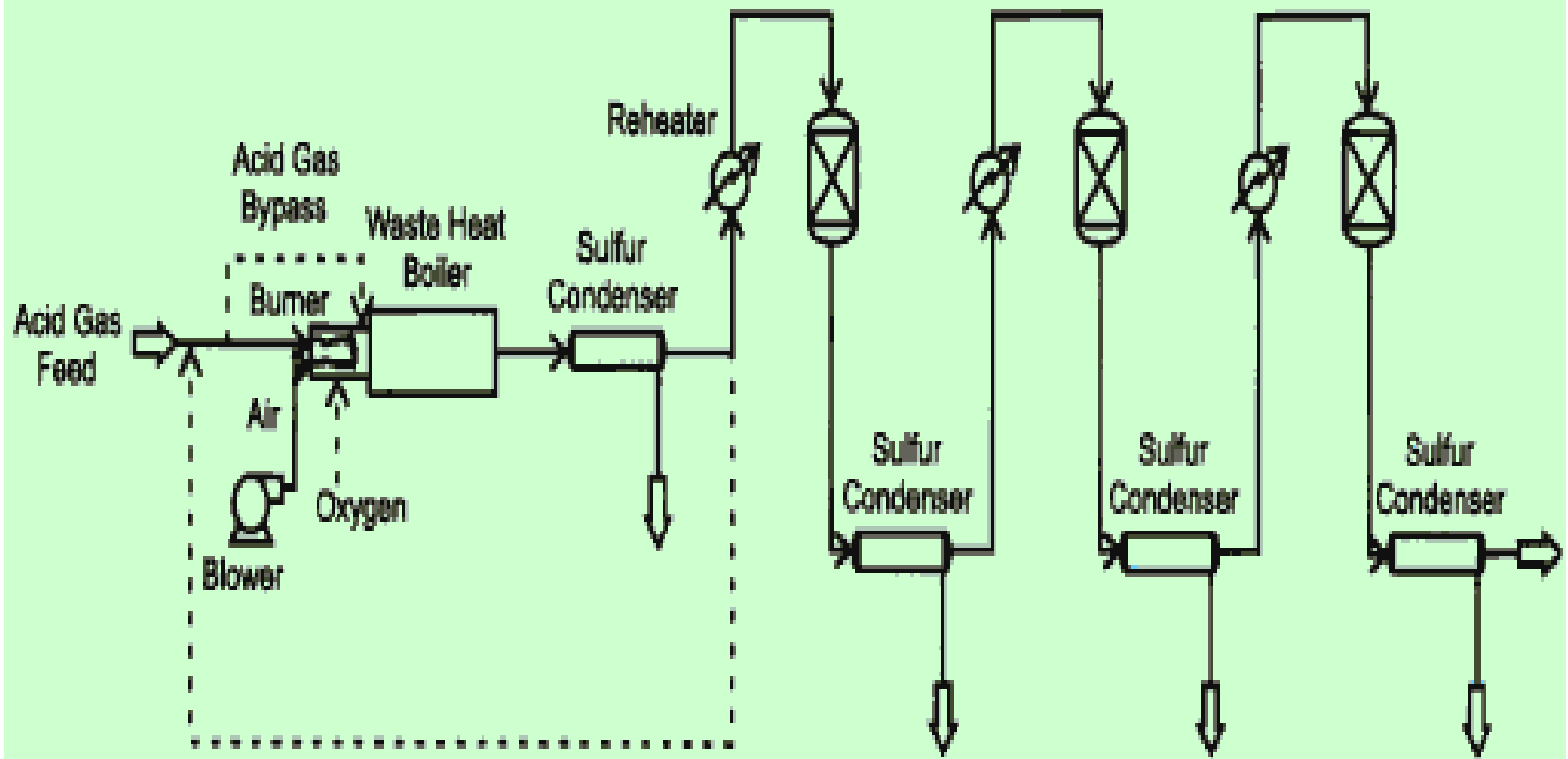
Figure 10.1. Schematic drawing of a typical amine treating unit.



CLAUS



Claus Catalyst Beds



Cope or Selectox Recycle

Courtesy of BR&E
www.bre.com

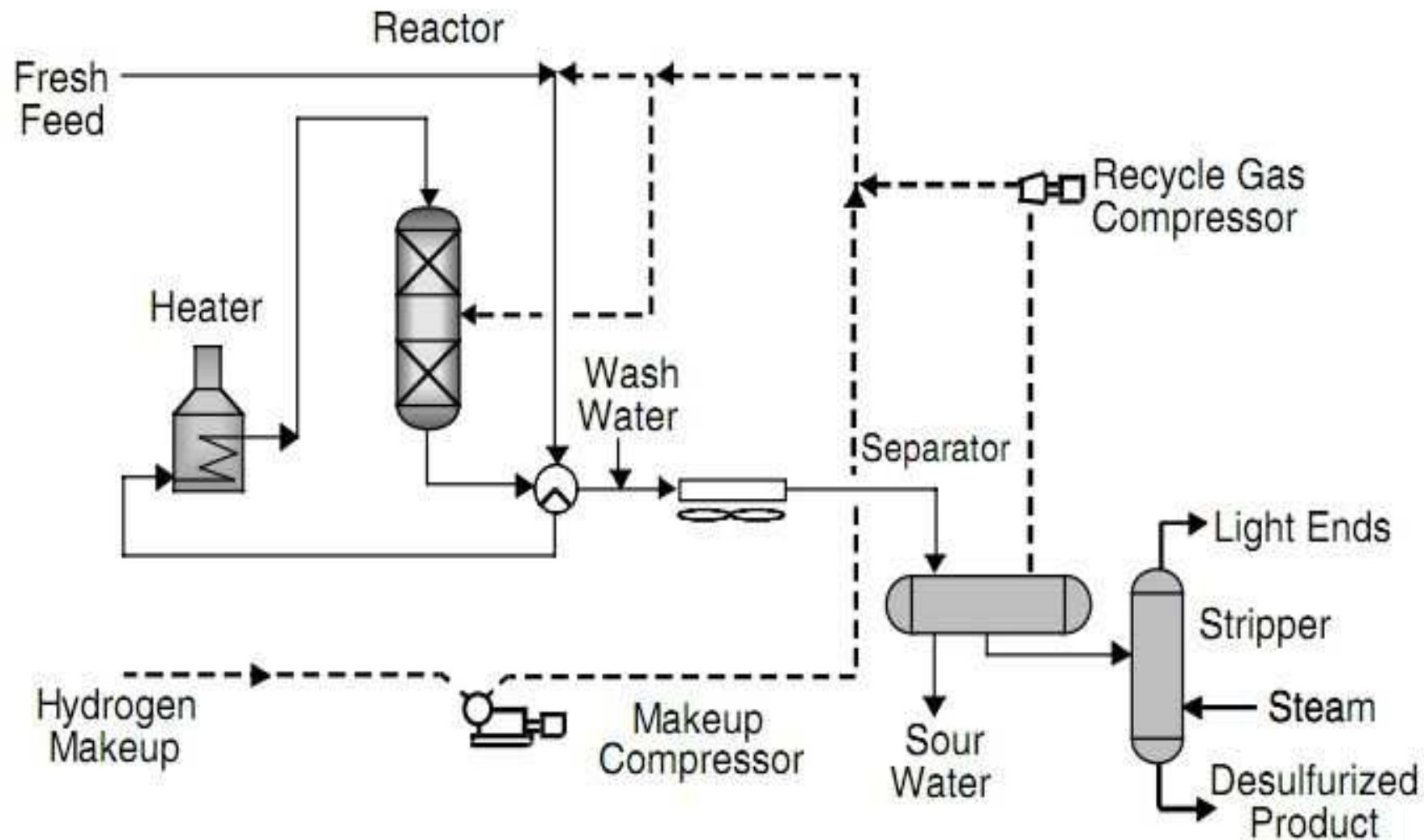
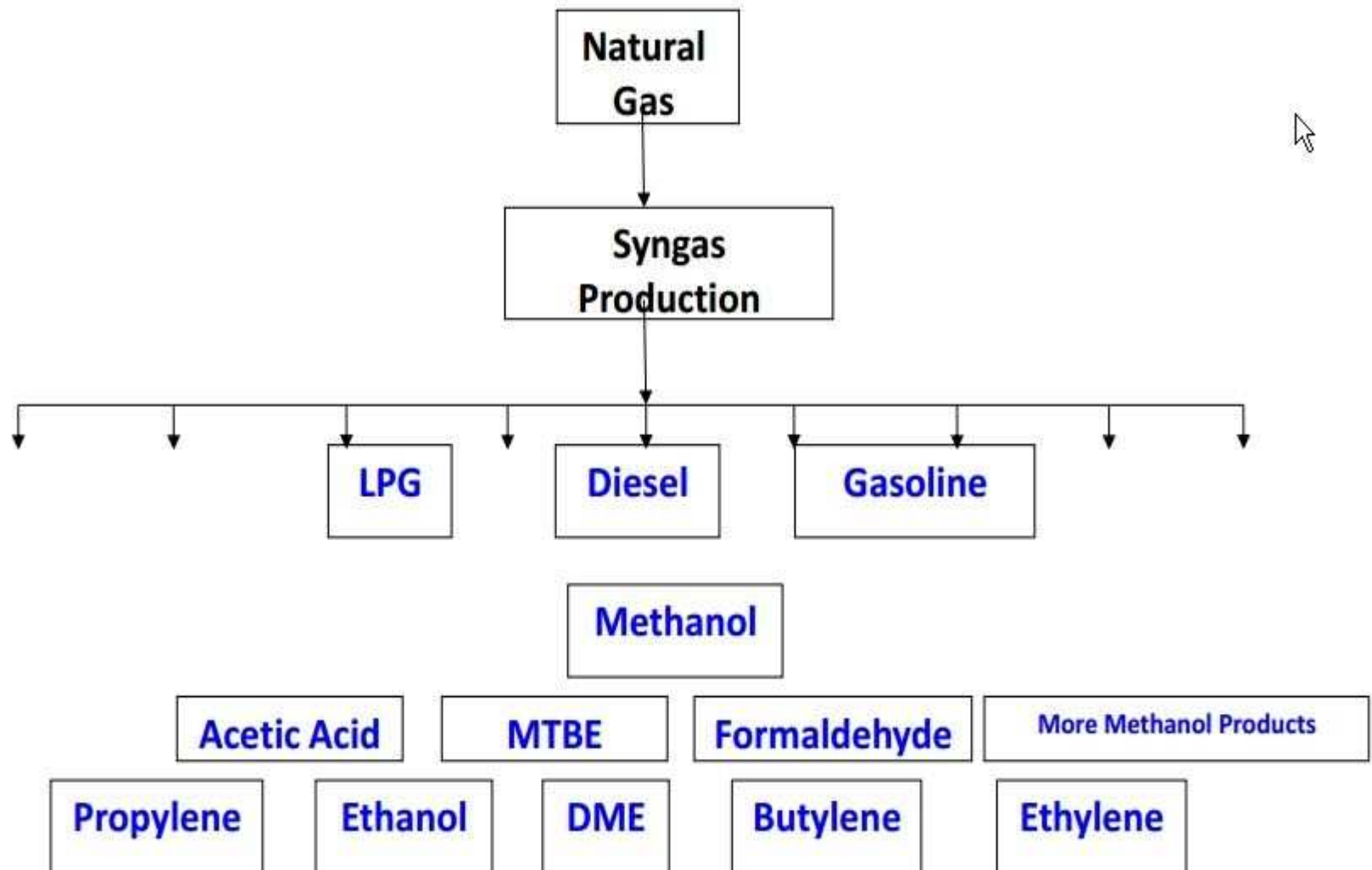


Figure 5.3. Naphtha hydrotreater flow scheme.

מוצרים מגז טבעי



Coal to fuels

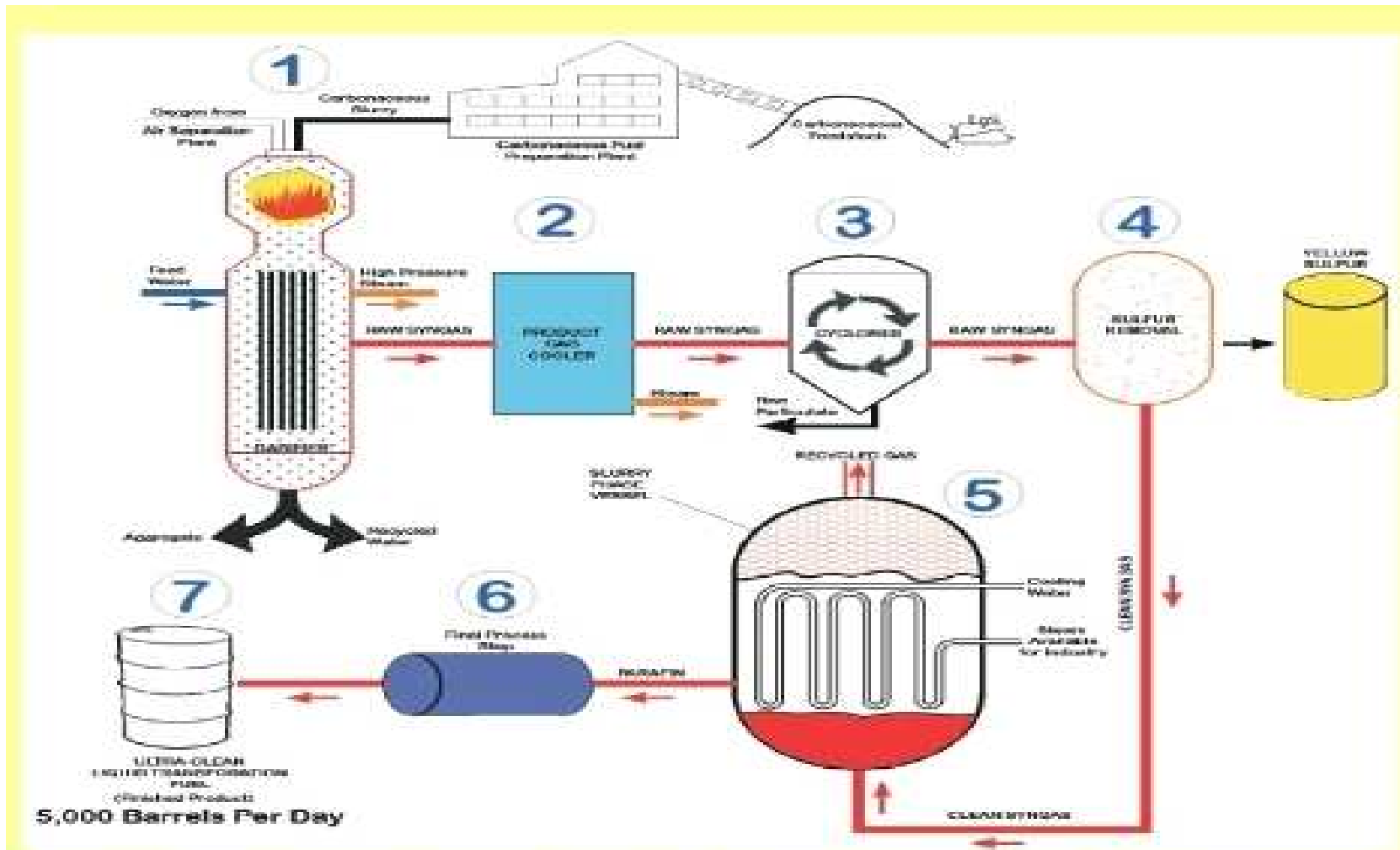
Raw materials

- Coal (high quality) •
- Coal (low quality- lignite) •
- Shale •
- Bituminous sands •

Processes

- Coal to liquids •
- Coal to syngas •
- Syngas to electricity •
- Syngas to fuels •

Coal to liquids pilot plant



The US Department of Energy (DOE) had an active coal liquefaction program in the 1990's (Summary Report, 2004: DOE Clean Coal Technology).

Syngas

Early Gasification Milestones

Date	Milestone
1790s	William Murdoch experiments with various types of gas, settling on coal gas as the most effective
1804	Coal gas first patented for lighting
1813	London and Westminster Gas Light & Coke Company illuminates Westminster Bridge with "town gas" lights on New Year's Eve using wooden pipes
1816	Baltimore, Maryland becomes the first U.S. city to light streets with "town gas"
1800s	"Town gas" lighting in factories replaces candles and lanterns, making the night shift possible and ushering in the Industrial Age

Table 2.3 Typical coal liquefaction processes

Process	Typical catalyst	Conditions		Hydrogenation		Comments
		T (°C)	P (atm)	Prime source	Method	
Bergius (original process developed early 1900s)	Iron oxide	465	200	H ₂	in liquefaction reactor	Most severe conditions; catalyst discarded
Solvent Refined Coal (Gulf Oil)	Minerals in coal (none added)	450	140	H ₂	in liquefaction reactor	Recycle of portion of product liquid to reactor; lack of hydrogenation specificity
H-Coal® (Hydrocarbon Research Inc.)	CoO—MoO ₃ /Al ₂ O ₃	450	200	H ₂	in liquefaction reactor	Catalyst ages rapidly
Exxon Donor Solvent	Minerals in coal in liquefaction reactor CoO—MoO ₃ /Al ₂ O ₃ in separate hydrogenation reactor	450	140	Tetrafin in liquefaction reactor. Recycled after hydrogenation in separate reactor		Further hydrogenation of product liquids in separate reactor—catalyst deactivation slow. Typical product yields 0.3 to 0.4 te liquid/te coal feed
National Coal Board supercritical extraction	In separate hydrogenation reactor	350–450	100–200	H ₂ in separate reactor		Supercritical gas extraction of portion of coal with PhMe as solvent

Table 2.4 Gasification processes (commercially proven)*

Process	Conditions	Typical products (vol. %)				Comments
		CH ₄	H ₂	CO	CO ₂	
Lurgi	Fixed bed reactor ~1000°C; 30 atm	12	37	18	32	Production of by-product heavy tar (~1%) restricts coal to 'non-caking' types. 'Slagging Gasifier' under development by British Gas Corporation to enable the difficult 'caking' coals to be handled
Koppers-Totzek	Entrained bed reactor ~1800°C; 1 atm	—	34	51	12	Can handle all coals; high temperatures destroy heavy organic tar. 'Shell-Koppers' pressurized version (15–30 atm) under development
Winkler	Fluidized bed reactor ~900°C; 1 atm	3	42	36	18	Higher pressure process (15 atm) under development
Texaco	Entrained bed reactor ~1200°C; 20–80 atm					Commercially successful process for partial oxidation of fuel oil to synthesis gas being developed to handle coal as coal/water or coal/oil slurries

*The field of coal gasification is in a very active state of development. Nearly 20 other processes at various stages of development have been described; see A. Varma, 1978, *Chemical*

- **British Gas/Lurgi** The BGL process uses an oxygen-blown, moving-bed, slagging gasifier producing raw fuel at 980 F and 395 psia.
- **Destec** The Destec process uses a two stage oxygen blown, entrained flow gasifier producing raw fuel at 1900 F and 412 psia.
- **KRW** The KRW gasifier is air blown producing fuel at 1900 F and 400 psia.
- **Shell** The Shell process uses a dry feed, pressurized, oxygen-blown, entrained flow, slagging gasifier producing raw fuel at 1826 F and 352 psia.
- **Texaco** This is a pressurized, oxygen blown, slagging system producing raw fuel at 2500 F and 475 psia.
- **Transport** This gasifier is still in the developmental stage. Both air blown and oxygen-blown circulating bed reactors were studied using both coal and limestone thus reducing or possibly eliminating sulfur cleanup requirements. The gasifier was designed to produce 1657 F, 395 psia steam.



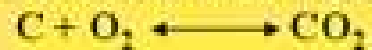
GASIFIER PROCESSES



Gasification with Oxygen



Combustion with Oxygen



Gasification with Carbon Dioxide



Gasification with Steam



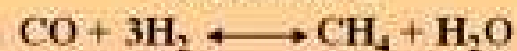
Gasification with Hydrogen



Water-Gas Shift



Methanation



Gasifier Gas
Composition
(Vol %)

H₂ 25 - 30

CO 30 - 60

CO₂ 5 - 15

H₂O 2 - 30

CH₄ 0 - 5

H₂S 0.2 - 1

COS 0 - 0.1

N₂ 0.5 - 4

Ar 0.2 - 1

NH₃ + HCN 0 - 0.3

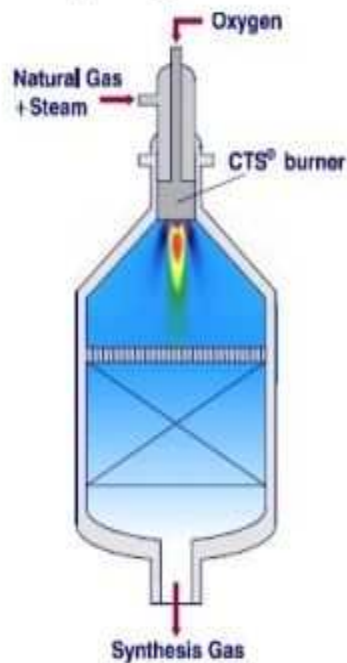
Ash/Slag/PM

עקרון ייצור חומרים שונים מגז טבעי הוא הפיכתו לסינגז (H₂ + CO), בעזרת קטאליזטור ייעודי:



$$\Delta H = + 206 \text{ kJ/mole}$$

Steam Reforming 1.1



טמפ': 800-850 °C , לחץ: 20-30 אטמ'.
קטאליזטור ניקל.
יחס CO/H₂ אופייני הוא 1:3

Autothermal Reforming (ATR) 1.2



$$\Delta H = - 36 \text{ kJ/mole}$$



$$\Delta H = + 206 \text{ kJ/mole}$$

יחס CO/H₂ אופייני הוא 1:2



Gasification R&D Areas and Major Technology Issues

Advanced Gasification

Fuel Feed System

- All ranks of coal
- Solid or slurry
- Injector reliability

Coal

Feed Water

Gasifier

- Single train reliability
- Refractory materials durability
- Alternate designs

High Pressure Steam

Instrumentation & Control

- Durability
- Accuracy
- On-line temperature measurement

Slag Residue

Air Separation

- Membrane durability
- Process integration
- No nitrogen in product

O₂

Gas Separation

Capture, Storage

CO₂

Syngas Separation (and Water-Gas Shift)

Fuels, Chemicals, Power

CO, H₂

Clean Syngas
CO/H₂

Shift Reactor, Converter

- Membrane durability
- Low flux
- Contaminant sensitivity
- Heat removal

Gas Cleaning

Raw Syngas

Process By-Products

- Heat Exchangers, Scrubbers, Filters
- Mild temperatures
- Multi-contaminant control
- Near-zero emissions
- Process integration & intensification

Cumulative Worldwide Gasification Capacity and Growth

MWth syngas

70,000

60,000

50,000

40,000

30,000

20,000

10,000

0

Note: 1 MWth=3,413,000 Btu/hr

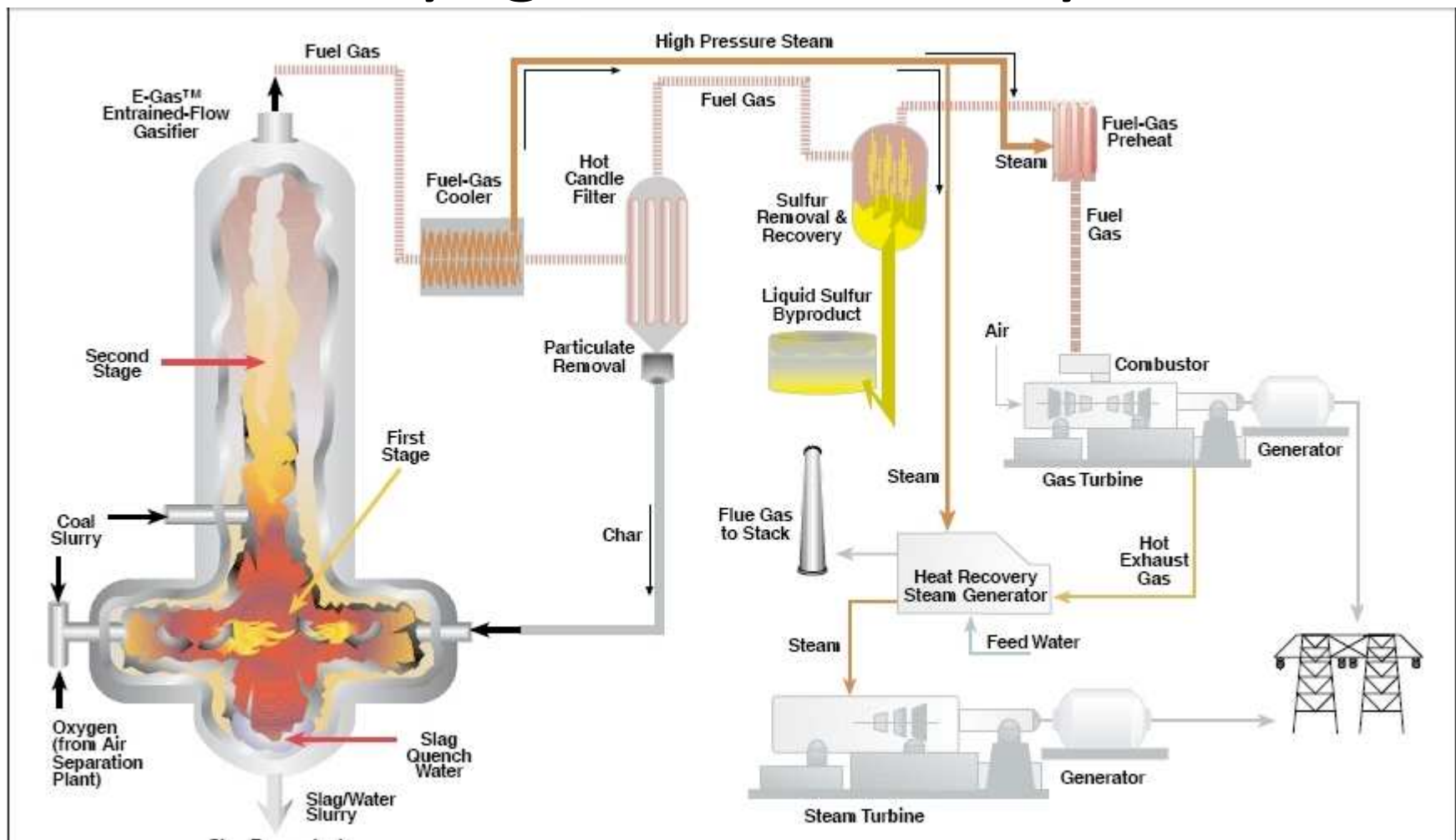
Planned

Real

1970 1972 1974 1976 1978 1980 1982 1984 1986 1988 1990 1992 1994 1996 1998 2000 2002 2004



Syngas to electricity



Syngas to crude

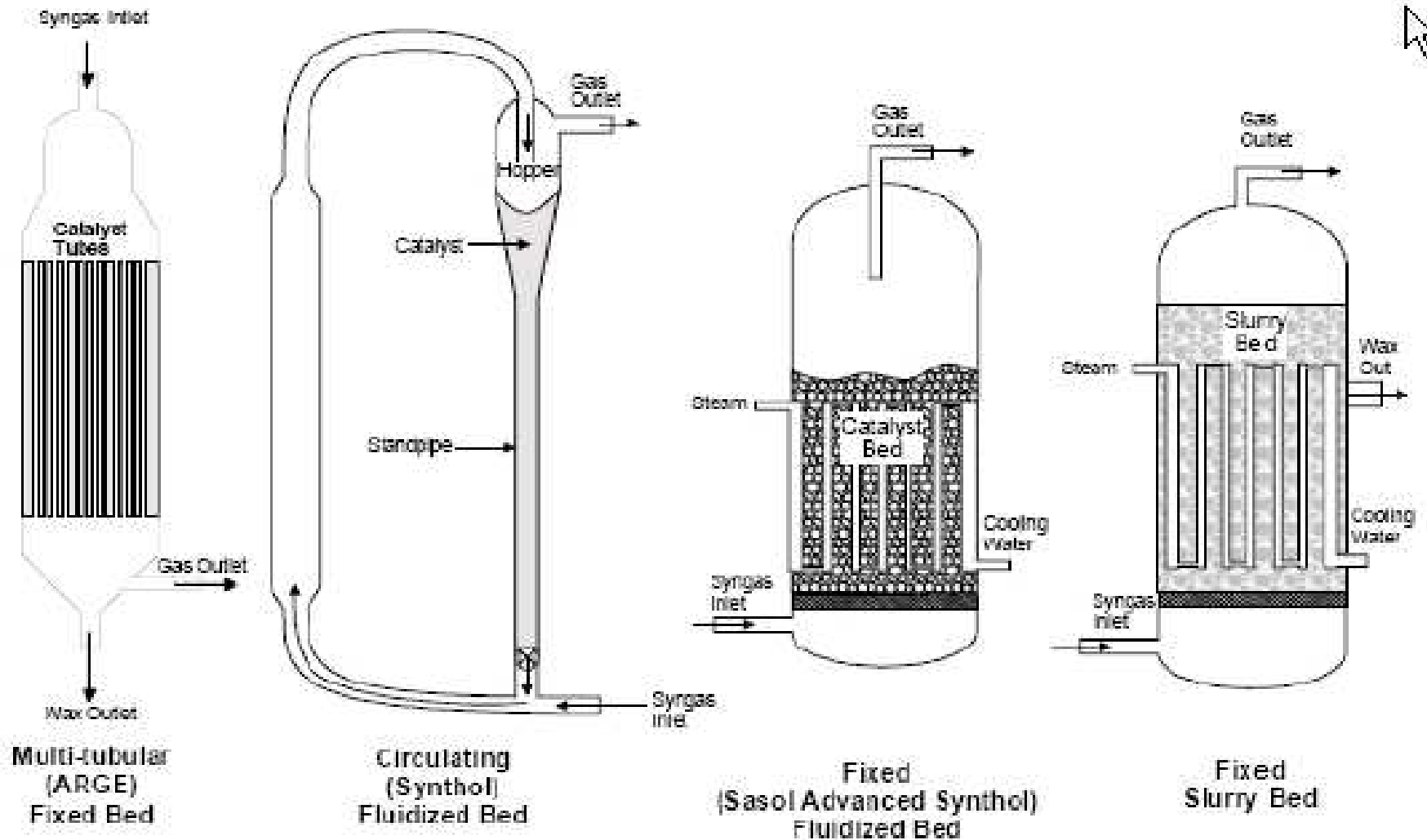


Figure 1: Types of FT reactors

Fischer Tropsch flowsheet

